

# Effect of thermophoresis and heat sources on hydro magnetic convective heat and mass transfer flow past a vertical wavy wall with variable viscosity, thermal conductivity, thermal radiation and Chemical reaction

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## I. INTRODUCTION:

The study of thermophoresis plays a vital role in the species transport mechanism of several devices consists of small micron sized particles and large temperature gradient. In fact, the particles are moving from hot surfaces to cold one. As small such particles (example dust) are suspended in a gas with a temperature gradient, experience a force in the direction opposite to the temperature gradient. The effect of the thermophoresis is so widespread in many practical applications in removing small particles from gas streams, in studying particles material deposition on turbine blades and in determining exhaust gas particle trajectories from combustion devices. This shows that thermophoresis is the dominant mass transfer mechanism in the modified chemical vapor deposition (MCVD) process as currently used in the fabrication of optical fiber performs. Thermophoretic deposition of radioactive particles is considered to be one of the important factors causing accidents in nuclear reactors

Several authors, Duwairi and Damseh et al [10], Damseh et al [7], Mahdy and Hady [21], Liu et al [20], Postelnicu [25], Dinesh and Jayaraj [9], Grosan et al [13], Tsai and Huang [34] have investigated the effect of thermophoresis in vertical plate, micro-channel, horizontal plate and parallel plate.

In light of these applications, the effect of thermophoresis in laminar flow of a viscous incompressible fluid was first established by Goren(12). We and Grief(36) studied the thermophoresis deposits including an application to the outside vapour deposits process. Talbolt et

al(33) analysed thermophoresis of particles in a heated boundary layer.

In recent years, considering the influence of thermophoresis, investigations on the free or mixed convection flow of viscous incompressible fluid past or along surface, vertical and horizontal surfaces, stretching sheet, wedge, cylinder and sphere under different boundary conditions have been accomplished by, Duwairi and Damseh et al [10], Damseh et al [7], Grosan et al(13), Mahdy and Hady [21], Liu et al [20], Jayaraj et al(17), Selim et al(29), Seddeek(28), Alam et al(1), Partha(8), Chen and Chan(24), Puvi Arasu et al(26), Das(8), Postelnicu(25), Sreenivasa Reddy et al(31,32), Ganesan et al(11), and Aliveni et al(2). But Wang and Chen(35) was the first investigated thermophoresis deposition of particles from a boundary layer flow onto a continuously moving wavy surface without considering the Darcy porous medium. In view of these applications.

With the fuel crisis deepening all over the world, there is a great concern to utilize the enormous power beneath the earth's crust in the geothermal region. Liquid in the geothermal region is an electrically conducting liquid because of high temperature. Hence the study of interaction of the geomagnetic field with the fluid in the geothermal region is of great interest, thus leading to interest in the study of MHD convection flows through porous medium.

The study of heat generation or absorption effects in moving fluids is important in view of several physical problems such as fluids undergoing exothermic or endothermic chemical reactions. The volumetric heat generation has been

assumed to be constant or a function of space variable. Bharathi et al [4] have discussed Non Darcy Hydromagnetic Mixed convective Heat and Mass Transfer flow of a viscous fluid in a vertical channel with Heat generating sources. Balasubramanyam et al [3] have discussed Non Darcy viscous electrically conductive Heat and Mass transfer flow through a porous medium in a vertical channel in the presence of heat generating sources. Hossain et al [15] studied the problem of natural convection flow along a vertical wavy surface with uniform surface temperature in the presence of heat generation or absorption. Hady et al [14] studied the problem of free convection flow along a vertical wavy surface embedded in electrically conducting fluid saturated porous media in the presence of internal heat generation or absorption effect.

Ling and Dybbs [19] has been investigated theoretically a very interesting effect to temperature dependent viscosity on free and mixed convective heat transport in a saturated porous medium. Hossain et al [16], Nasser et al [23] studied the effects of variable properties on natural convection along a vertical wavy surface without porous media. Mallikarjuna [22] have discussed the effect of thermophoresis on convective heat and mass transfer flow over a vertical wavy surface in a porous medium with variable properties.

In this paper, we investigate effect of heat sources on hydromagnetic flow of electrically conducting viscous fluid past a vertical wavy surface embedded in a fluid saturated porous medium with thermal radiation with variable properties. By employing the Runge-Kutta fourth order with Shooting technique, the governing equations have been solved. The effect of thermophoresis, heat sources, radiation, variable viscosity, thermal conductivity on the flow characteristics have been analysed. The obtained results are compared with those presented by Cheng (6) in the absence of heat source ( $Q=0$ ), magnetic field ( $M=0$ ), thermal radiation ( $Rd=0$ ), thermal conductivity ( $\beta=0$ ), thermophoresis ( $\tau=0$ ) and  $\theta_r \rightarrow \infty$ .

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0 \tag{2.2}$$

$$\frac{\partial}{\partial y} \left( \frac{\mu}{k} \bar{u} \right) - (\sigma \mu_e^2 H_o^2) \frac{\partial u}{\partial y} = \frac{\partial}{\partial x} \left( \frac{\mu}{k} \bar{v} \right) + \rho g (\beta_o \frac{\partial T}{\partial y} + \beta_1 T \frac{\partial T}{\partial y} + \beta_c \frac{\partial C}{\partial y}) \tag{2.3}$$

## II. FORMULATION OF THE PROBLEM:

We consider a steady, incompressible, two-dimensional laminar natural convective heat and mass transfer flow over a vertical wavy surface embedded in a saturated porous medium. The porous medium is uniform and local thermal equilibrium with the fluid. The Darcy law is used to describe the fluid saturated porous medium. The fluid is assumed to be gray, absorbing-emitting radiation but non-scattering medium. The wavy surface profile is given by

$$y = \bar{\sigma}(\bar{x}) = \bar{a} \sin\left(\frac{\pi \bar{x}}{l}\right) \tag{2.1}$$

where  $l$  is the characteristic length of wavy surface and  $\bar{a}$  is the amplitude of the wavy surface. The wavy surface is maintained at constant temperature  $T_w$  which are higher than the ambient fluid temperature  $T_\infty$ . We consider the natural convection-radiation flow in the presence of heat sources to be governed by the following equations under Boussinesq approximations:

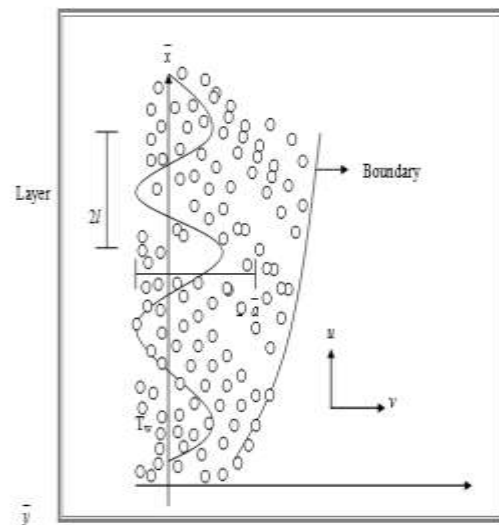


Fig. - 1: Physical Configuration and Co-ordinate System

$$\bar{u} \frac{\partial T}{\partial y} + \bar{v} \frac{\partial T}{\partial y} = \frac{\partial}{\partial x} \left( \alpha \frac{\partial T}{\partial x} \right) + \frac{\partial}{\partial y} \left( \alpha \frac{\partial T}{\partial y} \right) - \frac{1}{C_p} Q_H (T - T_\infty) - \frac{1}{C_p} \nabla \cdot q_r$$

(2.4)

$$u \frac{\partial C}{\partial x} + v \frac{\partial C}{\partial y} = D_b \left( \frac{\partial^2 C}{\partial x^2} + \frac{\partial^2 C}{\partial y^2} \right) - \frac{\partial}{\partial x} (U_T C) - \frac{\partial}{\partial y} (V_T C)$$

(2.5)

The relevant boundary conditions are

$$\bar{u} = 0, \bar{v} = 0, T = T_w, C = C_w \text{ at } \bar{y} = \bar{\sigma}(\bar{x}) = \bar{a} \text{Sin}\left(\frac{\pi \bar{x}}{l}\right)$$

$$\bar{u} \rightarrow 0, T \rightarrow T_\infty, C \rightarrow C_\infty \text{ as } \bar{y} \rightarrow \infty$$

(2.6)

where  $\bar{u}$  and  $\bar{v}$  are the volume averaged velocity components in the directions of x and y respectively, T, C are temperature, Concentration respectively;  $\rho$  is the density of the fluid,  $\mu$  is the dynamic viscosity of the fluid, k is the permeability of the porous medium,  $\sigma$  is the electrical conductivity,  $\mu_e$  is the magnetic permeability,  $H_0$  is the strength of the magnetic field, DB is the molecular diffusivity, kc is the coefficient of chemical reaction,  $\beta_o$  are the coefficients of thermal expansion,  $\alpha$  is the thermal conductivity,  $q_r$  is the radiative heat flux, g is the acceleration due to gravity and  $Q_H$  is the strength of the heat source. KT is the thermal diffusion ratio,  $T_m$  is the mean fluid temperature,  $U_T$  and  $V_T$  are thermophoretic velocities which can be written (see Wu and Greif (36))

$$U_T = -\frac{k v}{T_r} \frac{\partial T}{\partial x} \quad \text{and} \quad V_T = -\frac{k v}{T_r} \frac{\partial T}{\partial y}$$

(2.7)

$$k_{nf} = \frac{2C_s (\lambda_s / \lambda_p + C_1 k_n) [1 + k_n (C_1 + C_2 e^{-C_3 k_n})]}{(1 + 3C_m k_n)(1 + 2\lambda_g / \lambda_p + 2C_1 k_n)}$$

Where  $C_1, C_2, C_3, C_m, C_s$ , are constants,  $\lambda_g$  and  $\lambda_p$  are thermal conductivities of fluid and diffused particles, respectively and  $kn$  is the Knudsen number.

Where  $k$  is thermophoretic coefficient which ranges in the values between 0.2 and 1.2 and is defined as (See Talbot et al (33))

By applying Rosseland approximation (Brewster [5]) the radiative heat flux  $q_r$  is given by

$$q_r = -\left( \frac{4\sigma^*}{3\beta_R} \right) \frac{\partial}{\partial y} [T'^4]$$

(2.8)

Where  $\sigma^*$  is the Stephan – Boltzmann constant and mean absorption coefficient.

Assuming that the difference in temperature within the flow are such that  $T'^4$  can be expressed as a linear combination of the temperature. We expand  $T'^4$  in Taylor's series about  $T_e$  as follows

$$T'^4 = T_\infty^4 + 4T_0^3 (T - T_0) + 6T_0^2 (T - T_0)^2 + \dots$$

(2.9)

Neglecting higher order terms beyond the first degree in  $(T - T_\infty)$ . we have

$$T'^4 \cong -3T_0^4 + 4T_0^3 T$$

(2.10)

Differentiating equation (2.6) with respect to y and using (2.7) we get

$$\frac{\partial (q_r)}{\partial y} = -\frac{16\sigma^* T_0^3}{3\beta_R} \frac{\partial^2 T}{\partial y^2}$$

(2.11)

On using equations (2.11) in the last term of equation (2.4) we get

$$\bar{u} \frac{\partial T}{\partial y} + \bar{v} \frac{\partial T}{\partial y} = \frac{\partial}{\partial x} \left( \alpha \frac{\partial T}{\partial x} \right) + \frac{\partial}{\partial y} \left( \alpha \frac{\partial T}{\partial y} \right) - \frac{1}{C_p} Q_H (T - T_\infty) + \frac{16\sigma^* T_0^3}{C_p \beta_R} \left( \frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2} \right) + Ec \left( \frac{\partial^2 \psi}{\partial x^2} + \frac{\partial^2 \psi}{\partial y^2} \right)$$

(2.12)

The fluid properties are assumed to be constant except fluid viscosity and thermal conductivity. Therefore we assume that the viscosity of the fluid is to be an inverse function of the temperature and it can be expressed as [Lai and Kulacki [18]]

$$\frac{1}{\mu} = \frac{1}{\mu_\infty} (1 + \delta(T - T_\infty)) \text{ or } \frac{1}{\mu} = b((T - T_\infty)) \quad (2.13)$$

Where  $b = \frac{\delta}{\mu_\infty}$  and  $T = T_\infty - \frac{1}{\delta}$ . Both  $b$  and  $T_r$  are constants and their values depend on the reference state and the thermal property of the fluid i.e.  $\delta$ . In general  $b > 0$  for liquids and  $b < 0$  for gases,  $\theta_r$ , which is defined by

$$\theta_r = \frac{T_r - T_\infty}{T_w - T_\infty} = - \frac{1}{\delta(T_w - T_\infty)} \quad (2.14)$$

is constant. The parameter  $\theta_r$  was first introduced by Ling and Dyybs [19]. It is important to note that for  $\delta \rightarrow 0$  (i.e.  $\mu = \mu_\infty = \text{constant}$ ) then  $\theta_r \rightarrow \infty$ , the effect of viscosity is negligible. The value of  $\theta_r$  is determined by the temperature difference  $(T_w - T_\infty)$  and viscosity  $\delta$  of the fluid in consideration. A smaller value of  $\theta_r$  implies either the fluid viscosity changes considerably or the temperature difference is high. On the other hand, for a larger value of  $\theta_r$  implies either  $(T_w - T_\infty)$  or  $\delta$  is small, and therefore the effects of variable viscosity can be neglected. In either case the influence of variable viscosity plays a very important role and the liquid viscosity varies differently with temperature than that of gases. Therefore,  $\theta_r$  is positive for gases and negative for liquids respectively.

Also, we assume that the fluid thermal conductivity  $\alpha$  is to be varying as a linear function of temperature in the form [Seddeek and Salem [28]]

$$\alpha = \alpha_o (1 + E(T - T_\infty))$$

Where  $\alpha_o$  is the thermal diffusivity at the wavy surface temperature  $T_w$  and  $E$  is a constant depending on the nature of the fluid. It is worth mentioning here that  $E$  is positive for fluids such as air and  $E$  is negative for fluids such as lubrication oils. This can be written in the non-dimensional form [Slattery [30]] as

$$\alpha = \alpha_o (1 + \beta\theta) \quad (2.15)$$

Where  $\beta = E(T - T_\infty)$  is the thermal conductivity parameter. The variation of  $\beta$  can be taken in the range  $-0.1 \leq \beta \leq 0$  for lubrication oils,  $0 \leq \beta \leq 0.12$  for water and  $0 \leq \beta \leq 6$  for air.

In view of the continuity equation (2.2) we define the stream function  $\psi$  as

$$\bar{u} = \frac{\partial \bar{\psi}}{\partial y}, \quad v = - \frac{\partial \bar{\psi}}{\partial x} \quad (2.16)$$

In order to write the governing equations in the dimensionless form, we introduce the following non-dimensional variables as

$$x = \frac{\bar{x}}{l}, \quad y = \frac{\bar{y}}{l}, \quad a = \frac{\bar{a}}{l}, \quad \sigma = \frac{\bar{\sigma}}{l}, \quad \psi^* = \frac{\bar{\psi}}{l}, \quad \theta = \frac{T - T_\infty}{T_w - T_\infty},$$

$$\phi = \frac{C - C_\infty}{C_w - C_\infty} \quad (2.17)$$

The equations (2.12)-(2.15), equations (2.2), (2.3), and (2.10) reduce to

$$\left(\frac{1}{\theta - \theta_r}\right) \left(\frac{\partial \theta}{\partial y} \frac{\partial \psi^*}{\partial y} - \frac{\partial \theta}{\partial x} \frac{\partial \psi^*}{\partial x}\right) + \left(\frac{\partial^2 \psi^*}{\partial x^2} + \frac{\partial^2 \psi^*}{\partial y^2}\right) + Ra \left(1 - \frac{\theta}{\theta_r}\right) \left(\frac{\partial \theta}{\partial y}\right) (1 + 2\gamma_1 \theta)$$

$$+ N_r \left(\frac{\partial C}{\partial y}\right) - M^2 \frac{\partial^2 \psi^*}{\partial y^2} \quad (2.18)$$

$$\left(\frac{\partial \theta}{\partial x} \frac{\partial \psi^*}{\partial y} - \frac{\partial \theta}{\partial y} \frac{\partial \psi^*}{\partial x}\right) = \left(1 + \beta\phi + \frac{4Rd}{3}\right) \left(\frac{\partial^2 \theta}{\partial x^2} + \frac{\partial^2 \theta}{\partial y^2}\right) + \beta \left(\left(\frac{\partial \theta}{\partial x}\right)^2 + \left(\frac{\partial \theta}{\partial y}\right)^2\right) - Q\theta \quad (2.19)$$

$$Le \left( \frac{\partial \phi}{\partial x} \frac{\partial \psi^*}{\partial y} - \frac{\partial \phi}{\partial y} \frac{\partial \psi^*}{\partial x} \right) = \left( \frac{\partial^2 \phi}{\partial x^2} + \frac{\partial^2 \phi}{\partial y^2} \right) - Le \gamma \phi -$$

$$- Sc \tau \left( \frac{\partial^2 \theta}{\partial x^2} \phi + \frac{\partial^2 \theta}{\partial y^2} \phi + \frac{\partial \theta}{\partial x} \frac{\partial \phi}{\partial x} + \frac{\partial \theta}{\partial y} \frac{\partial \phi}{\partial y} \right) \quad (2.20)$$

Where  $Ra = \frac{\beta_T g (T_w - T_\infty) l}{\alpha_o \nu}$  is the Darcy-Rayleigh number,  $\nu = \frac{\mu_\infty}{\rho}$  is the kinematic viscosity of the

fluid,  $Rd = \frac{4\sigma^* T_\infty^3}{k_f \beta_R}$  is the Radiation parameter,  $Q = \frac{Q_H l^2}{\alpha_o C_p}$  is heat source parameter,  $M^2 = \frac{\sigma \mu_e^2 H_0^2 l^2}{\mu}$  is

the magnetic parameter.  $Le = \frac{\nu}{D_B}$  is the Lewis number,  $N = \frac{\beta_c (C_w - C_\infty)}{\beta_0 (T_w - T_\infty)}$ ,  $Ec = \frac{\mu (T_w - T_\infty)}{C_p}$  is

the Eckert parameter,  $\tau = -\frac{k}{T_r} (T_w - T_\infty)$  is the thermophoretic parameter and  $Sc = \frac{\nu}{D_B}$  is the Schmidt

number.

In equation(2.19),

$\tau = -\frac{k}{T_r} (T_w - T_\infty)$  represents thermophoresis

parameter. From the practical point view two possible cases exist, (i) heated surface ( $T_w - T_\infty > 0$ ), which leads to  $\tau < 0$ , (ii)

cold surfaces ( $T_w - T_\infty < 0$ ), which gives rise

$\tau > 0$ . For the second case thermophoresis is the special type of mechanism for capture of particles on cold surfaces, being especially important for submicron particles since thermophoresis velocity is relatively independent of particle, while the first one may be thought of suppose the particle deposition on the surface, it concludes that for heated surfaces a dust free stream is obtained adjacent to the surface due to particles moving away from the surface, thus fluid particle concentration is tending to zero near the surface. Hence thermophoretic velocity is treated as particle deposition velocity when  $\tau < 0$ .

The transformed boundary conditions are

$$\psi^* = 0, \theta = 1, \phi = 1 \text{ at } y = a \sin(x)$$

$$\frac{\partial \psi^*}{\partial y} \rightarrow 0, \theta \rightarrow 0, \phi \rightarrow \infty \text{ as } y \rightarrow \infty$$

(2.21)

We can transform the effect of wavy surface from the boundary conditions into the

governing equations by using suitable coordinate transformation with boundary layer scaling, for the case of free convection. The Cartesian coordinates (x, y) are transformed into the new variables ( $\xi, \eta$ ).

We incorporate the effect of effect of wavy surface and the usual boundary layer scaling into the governing equations (2.16) & (2.17) for free convection, using the transformations and  $Ra \rightarrow \infty$  (i.e boundary layer approximation),

$$x = \xi, \hat{\eta} = \frac{y - a \sin(x)}{\xi^{1/2} Ra^{-1/2}}, \psi^* = Ra^{1/2} \psi$$

(2.22)

These transformations are similar to those presented in, for instance, Rees and Pop [17]. We obtain the following boundary layer equations:

$$\left(\frac{1}{\theta - \theta_r}\right)(1 + a^2 \cos^2 \xi) \frac{\partial \theta}{\partial \eta} \frac{\partial \psi}{\partial \eta} + (1 + a^2 \cos^2 \xi) \frac{\partial^2 \psi}{\partial \eta^2} = Ra \xi^{1/2} \left(1 - \frac{\theta}{\theta_r}\right) \left(\frac{\partial \theta}{\partial \eta} + N \frac{\partial \phi}{\partial \eta}\right) - M^2 \frac{\partial^2 \psi}{\partial \eta^2} \quad (2.22)$$

$$\xi^{1/2} \left(\frac{\partial \theta}{\partial \xi} \frac{\partial \psi}{\partial \eta} - \frac{\partial \theta}{\partial \eta} \frac{\partial \psi}{\partial \xi}\right) = (1 + a^1 \cos^2(\xi)) \left(1 + \beta \phi + \frac{4Rd}{3}\right) \left(\frac{\partial^2 \theta}{\partial \eta^2}\right) + \beta \left(\frac{\partial \theta}{\partial \eta}\right)^2 - Q\theta \quad (2.23)$$

$$\xi^{1/2} Le \left(\frac{\partial \phi}{\partial \xi} \frac{\partial \psi}{\partial \eta} - \frac{\partial \phi}{\partial \eta} \frac{\partial \psi}{\partial \xi}\right) = (1 + a^2 \cos^2(\xi)) \left(\frac{\partial^2 \phi}{\partial \eta^2}\right) - Sc\tau \left(\frac{\partial^2 \theta}{\partial \xi^2} \phi + \frac{\partial^2 \theta}{\partial \eta^2} \phi + \frac{\partial \theta}{\partial \xi} \frac{\partial \phi}{\partial \xi} + \frac{\partial \theta}{\partial \eta} \frac{\partial \phi}{\partial \eta}\right) \quad (2.24)$$

### III. SOLUTION METHODOLOGY:

We now introduce the following similarity variables as

$$\eta = \frac{\bar{\eta}}{(1 + a^2 \cos^2(\xi))}, \psi = \xi^{1/2} f(\eta), \theta = \theta(\eta), \phi = \phi(\eta)$$

In equations(2.19)&(2.20),we obtain a system of ordinary differential equations as follows:

$$f'' + \left(\frac{1}{\theta - \theta_r}\right)\theta f' - \frac{M^2}{(1 + a^2 \cos^2 \xi)} f'' = Ra \left(1 - \frac{\theta}{\theta_r}\right) \left(\theta' + N \phi'\right) \quad (2.25)$$

$$\beta(\theta')^2 + \left(1 + \beta\theta + \frac{4Rd}{3}\right)\theta'' + \frac{1}{2} f\theta' - Q(1 + a^2 \cos^2(\xi))\theta \quad C_f = \frac{f''(0)(1 + a^2 \cos^2(\xi))Ra^{1/2}}{(1 + M^2 + a^2 \cos^2(\xi))} \quad (2.29)$$

$$Le\phi'' + \left(\frac{1}{2} Lef - Sc\tau\theta'\right)\phi' - Sc\tau\phi\theta'' = 0 \quad (2.27)$$

where prime denotes differentiation with respect to  $\eta$ .

The corresponding boundary conditions are

$$f = 0, \theta = 1, \phi = 1 \text{ at } \eta = 0 \quad (2.28)$$

$$f' \rightarrow 0, \theta \rightarrow 0, \phi \rightarrow 0 \text{ as } \eta \rightarrow \infty$$

In equation(2.26) the radiation parameter

$$Rd = \frac{4\sigma T_\infty^3}{k_f \beta_R} \text{ means that the rate of thermal}$$

radiation contribution relative to the thermal conditions. As  $Rd \rightarrow \infty$ , influence of thermal radiation is high in the boundary layer regime. For  $Rd \rightarrow 0$ , the term  $4Rd/3$  tends to zero. For  $Rd=1$ , thermal radiation and thermal conduction will give equal contribution.

The main results of practical interest in many applications are Skin friction coefficient  $C_f$ , heat transfer coefficient, mass transfer coefficient at the surface.

The skin friction coefficient  $C_f$  is given by

$$C_f = \frac{f''(0)(1 + a^2 \cos^2(\xi))Ra^{1/2}}{(1 + M^2 + a^2 \cos^2(\xi))} \quad (2.29)$$

The heat and mass transfer coefficients are expressed in terms of Nusselt and Sherwood numbers  $Nux$ ,  $Shx$ .

Nusselt number  $Nux$  and Sherwood number  $Shx$  are given by

$$Nux = \frac{xq_w}{\alpha_o (T_w - T_\infty)}, Shx = \frac{xm_w}{D_b (C_w - C_\infty)} \quad (2.24)$$

Where  $q_w$  is the heat flux on the wavy surface, and is defined by

$$q_w = -\alpha_0 \bar{n} \cdot \nabla T \text{ and } \bar{n} = \left( -\frac{a \cos(\xi)}{\sqrt{1+a^2 \cos^2(\xi)}}, \frac{1}{\sqrt{1+a^2 \cos^2(\xi)}} \right)$$

is the unit normal vector to the wavy surface,  $\alpha_0$  is the effective porous medium thermal conductivity. Therefore

$$Nu_\xi = -\frac{\theta'(0) Ra_\xi^{1/2}}{\sqrt{1+a^2 \cos^2(\xi)}},$$

$$Sh_\xi = -\frac{\phi'(0) Ra_\xi^{1/2}}{\sqrt{1+a^2 \cos^2(\xi)}} \quad (2.30)$$

#### IV. COMPARISON

Comparison the values of the rate of heat and mass transfer with values reported by Cheng(6) for  $\beta=0, \tau=0, Q=0, Rd=0, M=0$  and  $\theta r \rightarrow \infty$ .

Parameters	NuxRa <sup>-1/2</sup>	ShxRa <sup>-1/2</sup>	NuxRa <sup>-1/2</sup>	ShxRa <sup>1/2</sup>
Le	N	Cheng(6)		Present results
1	4	0.992	0.992	0.9943
10	4	0.681	3.290	0.6815
10	4	0.521	10.521	0.5222
4	1	0.559	1.358	0.5592
4	2	0.650	1.624	0.6501
4	3	0.728	1.852	0.7282

Comparison the values of the rate of heat and mass transfer with values reported by Mallikarjuna(22) for  $Q=0, M=0, Rd=0$

Parameters			NuxRa <sup>-1/2</sup>	ShxRa <sup>-1/2</sup>	NuxRa <sup>-1/2</sup>	ShxRa <sup>1/2</sup>
$\theta r$	$\beta$	$\tau$	Mallikarjuna(22)		Present results	
-2.0	0.5	1.0	0.585	0.465	0.5849	0.4648
-4.0	0.5	1.0	0.534	0.434	0.5399	0.4339
-10.0	0.5	1.0	0.475	0.412	0.4748	0.4110
-2.0	1.0	1.0	0.605	0.494	0.6048	0.4938
-2.0	1.5	1.0	0.595	0.483	0.5951	0.4836

-2.0	2.0	1.0	0.592	0.472	0.5921	0.4722
-2.0	0.5	1.0	0.595	0.395	0.5945	0.3948
-2.0	0.5	2.0	0.605	0.345	0.6047	0.3449
-2.0	0.5	2.0	0.615	0.295	0.6112	0.2948

In the absence of mass transfer(N=0) and heat sources(Q=0) and magnetic field(M=0) the results are in good agreement with Mallikarjuna[22]

#### V. RESULTS AND DISCUSSION:

Figs.2a-2c illustrate the variation of velocity, temperature and concentration with Grashof number(G). It can be observed from the profiles that the axial velocity enhances in the flow region with increasing G. An increase in G reduces the temperature and concentration. This may be attributed to the fact that the thickness of the thermal and solutal boundary layers reduce with increasing values of G.

Figs.3a-3c depict the variation of velocity, temperature and concentration with magnetic parameter(M). From the profiles we find that the velocity reduces with G in the entire flow region. The temperature and concentration enhance with increasing values of magnetic parameter. This may be attributed to the fact that the thickness of the thermal and solutal boundary layer decay with increasing M.

Figs.5a-5c represent u,  $\theta$  and  $\phi$  with heat source parameter(Q). From fig.5a, we find that an increase in the strength of the heat generating source enhances the velocity in the region(0,1.0) adjacent to the wall and reduces far away from the wall, while in the case of heat absorbing source, heat is generated in the region(0,1.0) and the heat energy is absorbed in the region(1.0,4.0). The temperature and the concentration decrease with increase in  $Q>0$  and enhance with increase in  $Q<0$  (fig. 5b&5c).

Figs.6a-6c show the variation of velocity and temperature with the influence of radiation parameter(Rd). From fig.6a we find that the velocity reduces in the flow region(0,1.0) and enhances far away from the boundary. This means that the thickness of the momentum boundary layer reduces with increasing values of Rd. Fig.6b&6c represents the temperature and concentration with Rd. It can be seen from the profiles that an increase in Rd leads to thickening of the thermal and solutal boundary layers which results in an enhancement of the temperature and concentration in the flow region.

The variation of non-dimensional velocity and temperature profiles with  $\eta$  for different values of temperature dependent viscosity parameter ( $\theta_r$ ) is illustrated in figs.7a-7c. It is found that from fig.7a that the velocity of the fluid reduces in the region (0,2.0) and enhances far away from the wall. This can be explained physically as the parameter  $\theta_r$  increases there is increment in the boundary layer thickness. From fig.7b&7c we notice that the temperature and concentration profiles increase with increasing values of  $\theta_r$ . This can be attributed to the fact that an increase in  $\theta_r$  grows the thickness of the thermal and solutal boundary layers which results in an enhancement of the temperature and concentration in the flow region.

Figs.8a-8c represent the effect of thermal conductivity parameter  $\beta$  on the non-dimensional velocity, temperature and concentration. Fig.8a shows the variation of velocity with  $\beta$ . In this case the velocity is found to depreciate in the flow region (0,1.0) adjacent to the wall and enhances far away from the wall. From fig.8b we found that as the thermal conductivity parameter  $\beta$  increases the temperature enhances. This is due to the thickening of the thermal boundary layer as a result of increasing values of thermal conductivity. From fig.8c we found that as the thermal conductivity parameter  $\beta$  decreases the concentration reduces in the entire flow region. This is due to the thinning of the solutal boundary layer as a result of increasing values of thermal conductivity.

The effect of thermophoretic parameter ( $\tau$ ) on  $u, \theta$  and  $\phi$  can be seen from the figs.9a-9c. From fig.9a we find that increasing the thermophoretic parameter ( $\tau$ ) tends to increase significantly i.e. increase the thickness of the momentum boundary layer. Fig.9c reveals that the temperature profile depreciates considerably with increase in  $\tau$ . From fig.9c it is seen that increase in thermophoretic parameter ( $\tau$ ) leads to raise the values of concentration. In other words, increase in  $\tau$  decelerates the thermal boundary layer thickness while accelerates the solutal boundary layer thickness.

From figs.10a-10c we notice that an increase in Schmidt number ( $Sc$ ) increases the velocity in the narrow region (0,0.5) and in the remaining region it reduces. Lesser the molecular diffusivity larger the temperature and smaller the concentration in the flow region (figs.10b&10c). In other words, an increase in  $Sc$  decays the momentum boundary layer in (0,0.5) and decays in the region (0.5,4.0). Also the thermal boundary layer

grows and the solutal layer decays with increasing  $Sc$ .

Figs.11a-11c represent  $u, \theta$  and  $\phi$  with amplitude of the wavy surface 'a'. From fig.11a, we find that an increase in amplitude reduces the velocity in the entire flow region. The temperature and concentration increase with increase in 'a' in the entire flow region.

Figs.12a-12c depict the variation of  $u, \theta$  and  $\phi$  with streamwise coordinate ( $\xi$ ). It can be seen from the profiles that an increase in streamwise coordinate increases the velocity and reduces the temperature, concentration in the flow region.

The skin friction ( $C_f$ ) at the wall is represented in table.2 for different variations. From the tabular values we find that the magnitude of the skin friction enhances with increase in  $Re$  and  $M_i |C_i|$  increases at the wall with increase in buoyancy ratio ( $Nr > 0$ ) when the buoyancy forces are in the same direction and for the forces acting in opposite directions,  $C_f$  reduces with  $Nr < 0$ . Higher the viscosity parameter ( $\theta_r$ ) or higher thermal radiation ( $R_d$ ) or thermophoretic parameter ( $\tau$ ) smaller the skin friction at the wall. An increase in thermal conductivity ( $\beta$ ) leads to an enhancement in  $C_f$ . Higher the strength of the heat generating/absorbing heat source larger the magnitude of  $C_f$  at the wall. Lesser the molecular diffusivity Lewis number ( $Le$ ) or stream wise coordinate ( $\xi$ ) larger the skin friction at the wall. Also an increase in amplitude of the wavy surface 'a' leads to a depreciation in the magnitude of  $C_f$  at the wall.

The rate of heat transfer ( $Nu$ ) at the wall is displayed in table.1. From the tabular values we find that rate of heat transfer at the wall increases with increase in Grashof number ( $G$ ) or magnetic parameter ( $M$ ). Increasing buoyancy ratio ( $Nr > 0$ ) enhances the rate of heat transfer ( $Nu$ ) when the buoyancy forces are in the same directions and for the forces acting in opposite directions we find a reduction in  $Nu$  at the wall. The Nusselt number reduces with increase in viscosity parameter ( $\theta_r$ ). The variation of  $Nu$  with heat generating source parameter ( $Q > 0$ ) and reduces with heat absorbing source ( $Q < 0$ ). The Nusselt number reduces with increase in  $R_d$ . An increase in thermal conductivity parameter ( $\beta$ ) / thermophoretic parameter ( $\tau$ ) increases the Nusselt number at the wall. The rate of heat transfer at the wall grows with increasing  $Sc$ . The variation of  $Nu$  with amplitude of the wavy surface (a) and streamwise coordinate ( $\xi$ ) shows that  $Nu$  decreases with increase in 'a' and enhances with ' $\xi$ '.



The rate of mass transfer( $Sh$ ) at the wall is displayed in table.1.From the tabular values we find that rate of heat transfer at the wall increase with increase in  $G$  or  $M$  at the wall.Increasing buoyancy ratio( $Nr$ ) enhances  $Sh$  when the buoyancy forces are in the same directions and for the forces acting in opposite directions we find a reduction in  $Sh$  at the wall..The Sherwood number reduces with increase in viscosity parameter( $\theta_r$ ).The variation of  $Sh$  with heat source parameter( $Q$ ) shows that  $Sh$  increases with increase in heat generating/absorbing heat source. The Sherwood number enhances with increase in  $Rd$  or thermal conductivity parameter( $\beta$ ).An increase in thermophoretic parameter( $\tau$ ) depreciates the rate of mass transfer at the wall.The rate of mass transfer  $Sh$  at the wall decays with increase in  $Sc$ .The variation of  $Sh$  with amplitude of the wavy surface (a) and streamwise coordinate( $\xi$ ) shows that  $Sh$  decreases with increase in 'a' and enhances with ' $\xi$ '.

Parameter	$\tau(0)$	$Nu(0)$	$Sh(0)$	
R a	2	-2.04921	0.647698	0.696629
	4	-5.68454	0.852137	1.049233
	6	-10.3421	1.00824	1.317239
	10	15.4116	1.25569	1.740933
M	0.5	-1.67621	0.421996	0.755057
	1.0	-1.75005	0.427222	0.769116
	1.5	-1.92645	0.439276	0.801253
	2.0	3.6587	0.459794	0.855098
N r	1.0	-0.7438	0.502399	0.445801
	2.0	-1.57612	0.603067	0.619884
	-0.5	-0.268699	0.356704	0.206066
	-1.5	-0.119499	0.219677	0.031379
Q	0.5	-2.15126	0.513385	0.656064
	1.5	-2.30398	0.566705	0.679954
	-0.5	-1.32029	0.159097	0.662008
	-1.5	-1.39044	0.146142	0.741572
R d	0.5	-2.15126	0.513385	0.656064
	1.5	-2.01417	0.436305	0.694776
	3.5	-1.96932	0.408784	0.706148
	5.0	-1.85545	0.360287	0.710648
S c	0.2	-1.71636	0.420728	0.793261
	4			
	0.6	-1.67621	0.421996	0.755057

	6			
	1.3 0	-1.57667	0.425086	0.660461
	2.0 1	2.92989	0.428004	0.569004
	-2.0	-0.910404	0.520194	0.476496
$\theta_r$	-4.0	-0.796641	0.508911	0.457001
	-6.0	-0.765534	0.505261	0.450718
	-			
	10. 0	-0.79865	0.502399	0.445801
$\beta$	0.5	-2.15124	0.513385	0.656064
	1.0	-2.17654	0.514721	0.677219
	1.5	-2.18976	0.515567	0.698765
	2.0	-2.224567	0.5178965	0.712345
$\tau$	0.2	-1.67621	0.421996	0.755057
	0.4	-1.60362	0.424257	0.686055
	0.6	-1.53911	0.426232	0.624803
	0.8	2.92951	0.428134	0.564868
a	0.1	-1.51648	0.335793	0.762992
	0.2	-1.51579	0.335749	0.762846
	0.3	-1.51479	0.335686	0.762632
	0.5	2.90888	0.335505	0.762022
$\xi$	$\pi \square$ 6	-1.51637	0.335787	0.76297
	$\pi \square$ 4	-1.51648	0.335793	0.762992
	$\pi \square$ 3	-1.51658	0.3358	0.763014
	$\pi \square$	2.91561	0.335806	0.763036
	$\square$			

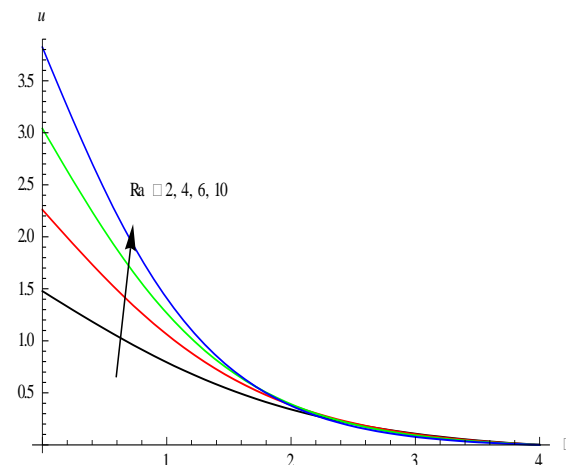
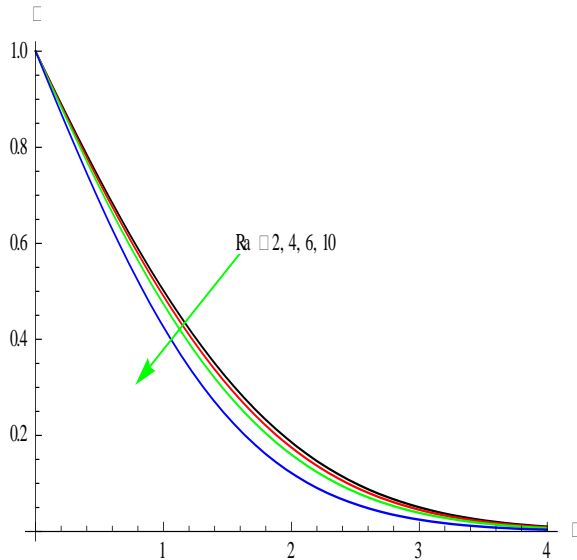
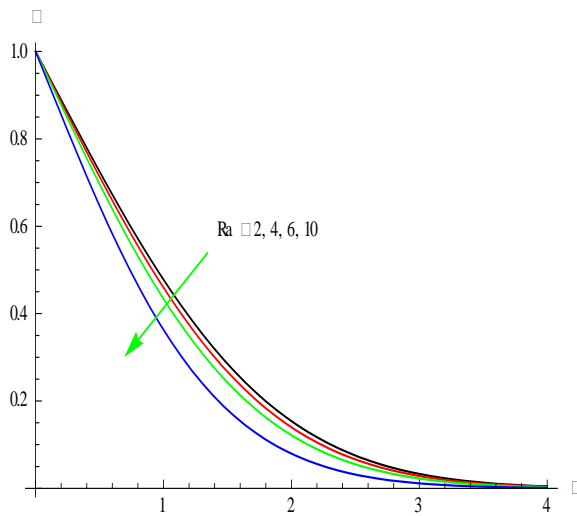


Fig.2a variation of axial velocity(u)with Ra

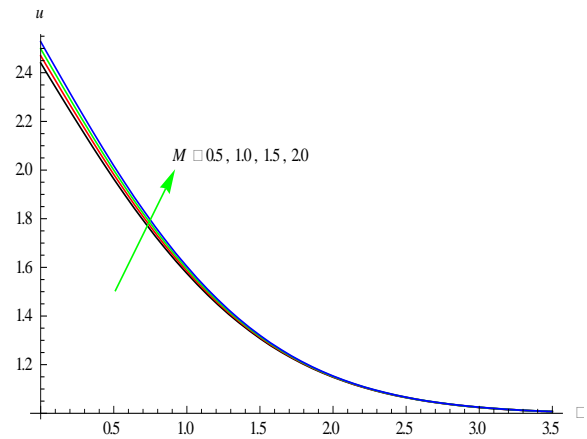
$M=0.5, Nr=0.5, Rd=0.5, \beta=0.5, \theta_r=-2,$   
 $Sc=0.24, a=0.2, \xi=\pi/4$



**Fig.2b** variation of temperature( $\theta$ )with Ra  
 $M=0.5, Nr=0.5, Rd=0.5, \beta=0.5, \theta_r=-2,$   
 $Sc=0.24, a=0.2, \xi=\pi/4$

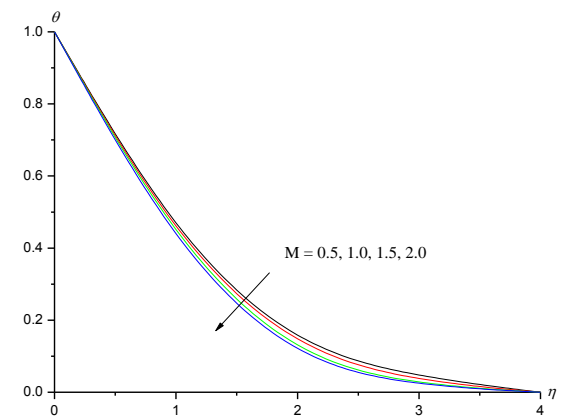


**Fig.2c** variation of Concentration( $\phi$ ) with Ra  
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 $Sc=0.24, a=0.2, \xi=\pi/4$

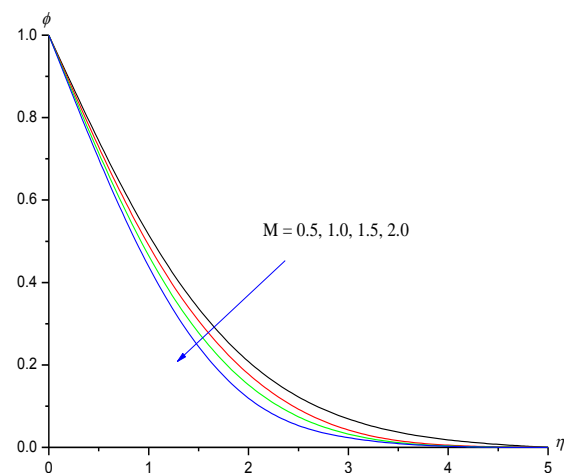


**Fig.3a** variation of axial velocity( $u$ )with M

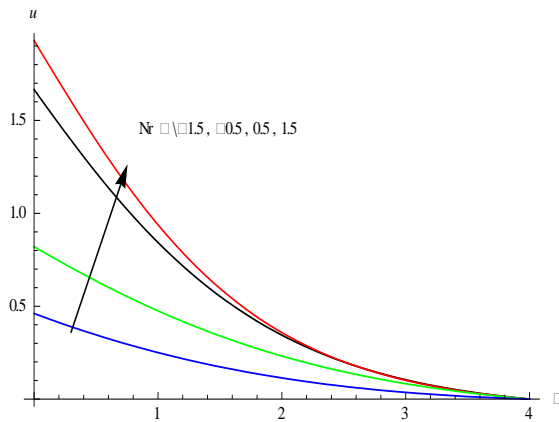
$Ra=2.0, Nr=0.5, Rd=0.5, \beta=0.5, \theta_r=-2,$   
 $Sc=0.24, a=0.2, \xi=\pi/4$



**Fig.3b** variation of temperature( $\theta$ )with M  
 $Ra=2.0, Nr=0.5, Rd=0.5, \beta=0.5, \theta_r=-2,$   
 $Sc=0.24, a=0.2, \xi=\pi/4$

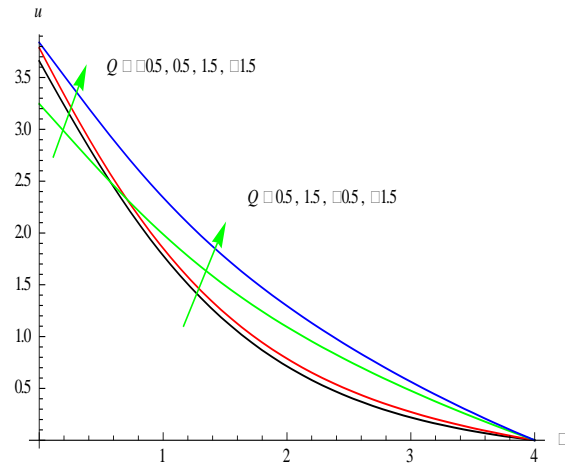


**Fig.3c** variation of Concentration( $\phi$ )with M  
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 $Sc=0.24, a=0.2, \xi=\pi/4$

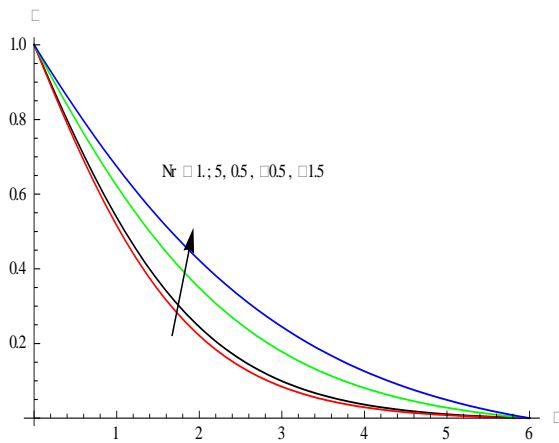


**Fig.4a** variation of axial velocity( $u$ )with  $Nr$   
 $M=0.5, Ra=2.0, Rd=0.5, \beta=0.5, \theta_r=-2,$   
 $Sc=0.24, a=0.2, \xi=\pi/4$

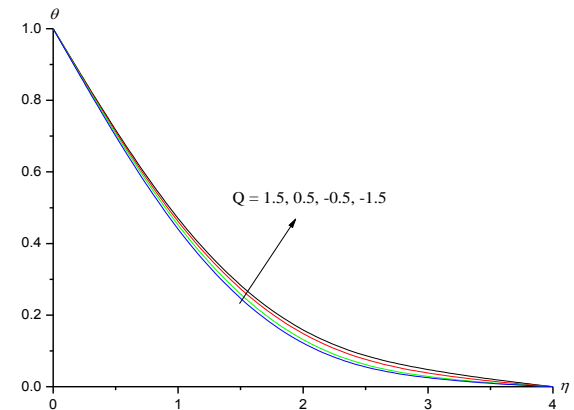
$Sc=0.24, a=0.2, \xi=\pi/4$



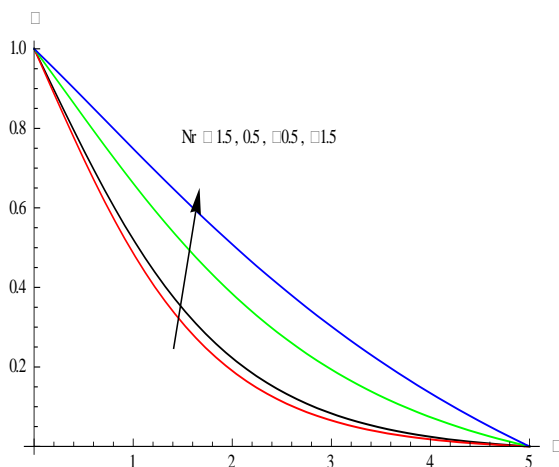
**Fig.5a** variation of axial velocity( $u$ )with  $Q$   
 $Ra=2.0, M=0.5, Nr=0.5, Rd=0.5, \beta=0.5, Sc=0.24,$   
 $\theta_r=-2, a=0.2, \xi=\pi/4$



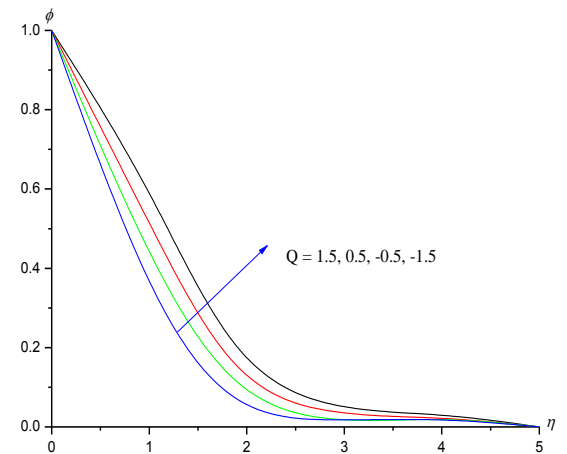
**Fig.4b** variation of temperature( $\theta$ )with  $Nr$   
 $Ra=2.0, M=0.5, Rd=0.5, \beta=0.5, \theta_r=-2,$   
 $Sc=0.24, a=0.2, \xi=\pi/4$



**Fig.5b** variation of temperature( $\theta$ )with  $Q$   
 $Ra=2.0, Nr=0.5, Rd=0.5, \beta=0.5, Sc=0.24,$   
 $\theta_r=-2, a=0.2, \xi=\pi/4$

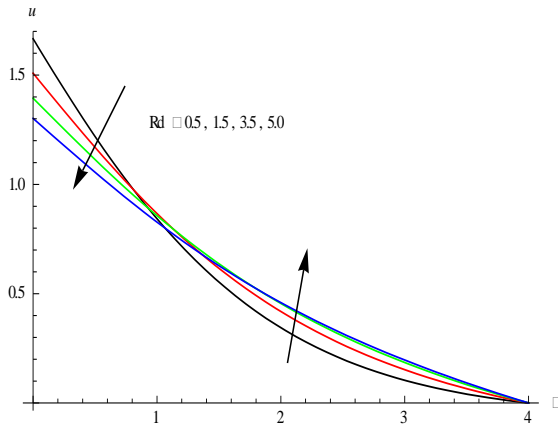


**Fig.4c** variation of Concentration( $\phi$ )with  $Nr$   
 $M=0.5, Ra=2.0, Rd=0.5, \beta=0.5, \theta_r=-2,$



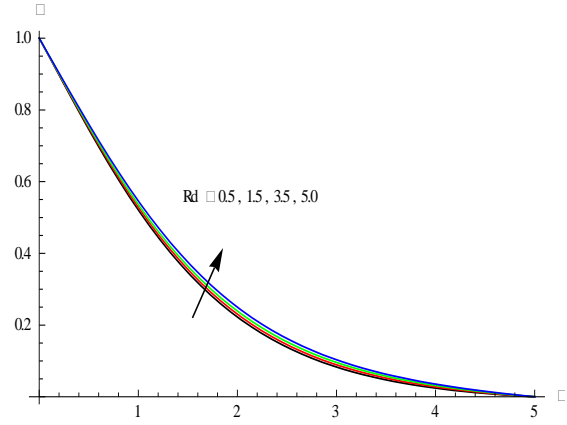
**Fig.5c** variation of Concentration( $\phi$ )with  $Q$   
 $M=0.5, Ra=2.0, Rd=0.5, \beta=0.5, Sc=0.24,$

$\theta_r = -2, a = 0.2, \xi = \pi/4$

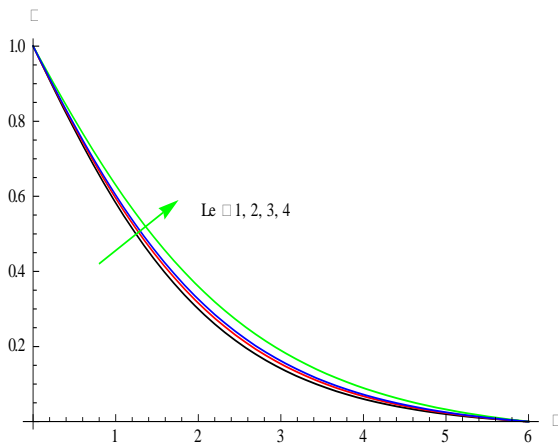


**Fig.6a** variation of axial velocity( $u$ )with  $Rd$   
 $M=0.5, Nr=0.5, M=0.5, \beta=0.5, Sc=0.24,$   
 $\theta_r = -2, a = 0.2, \xi = \pi/4$

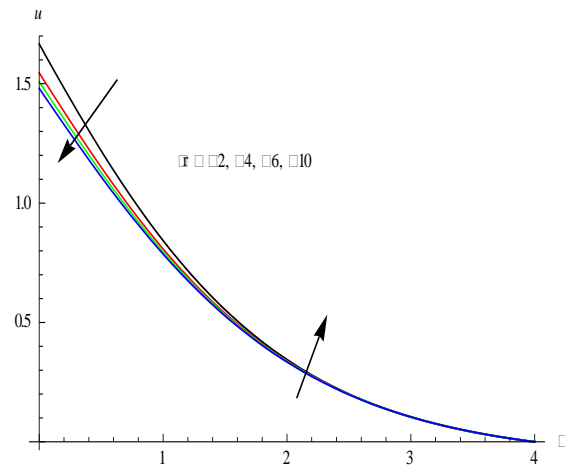
$Sc = 0.24, a = 0.2, \xi = \pi/4$



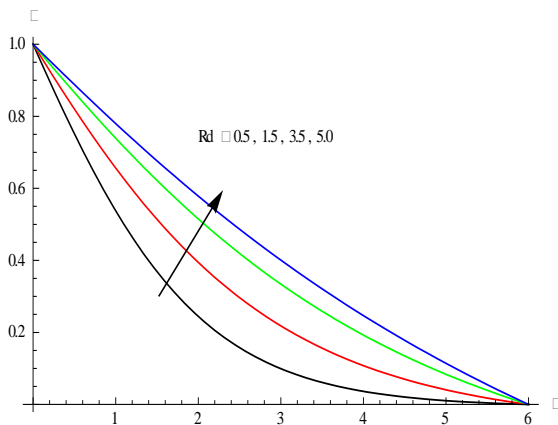
**Fig.6c** variation of Concentration( $\phi$ )with  $Rd$   
 $M=0.5, Ra=2.0, Ra=2.0, \beta=0.5, Sc=0.24,$   
 $\theta_r = -2, a = 0.2, \xi = \pi/4$



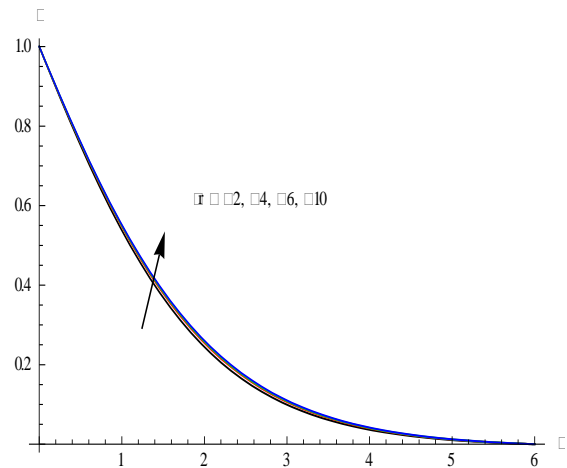
**Fig.6b** variation of temperature( $\theta$ )with  $Rd$   
 $M=0.5, Ra=2.0, \beta=0.5, \theta_r = -2,$   
 $Sc=0.24, a = 0.2, \xi = \pi/4$

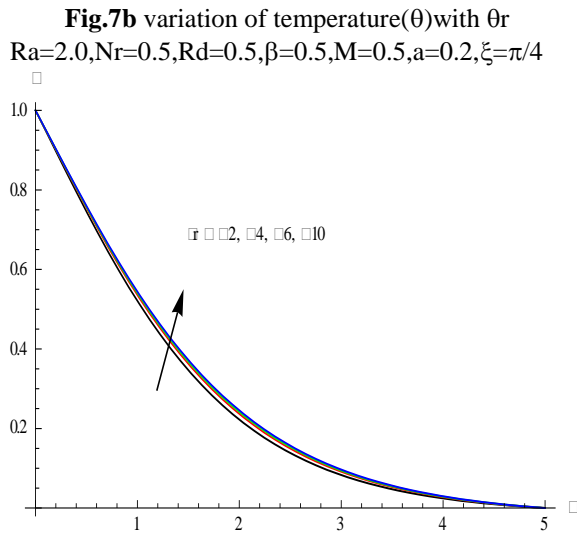


**Fig.7a** variation of axial velocity( $u$ )with  $\theta_r$   
 $M=0.5, Nr=0.5, Rd=0.5, \beta=0.5, Sc=0.24,$   
 $Ra=2, a = 0.2, \xi = \pi/4$

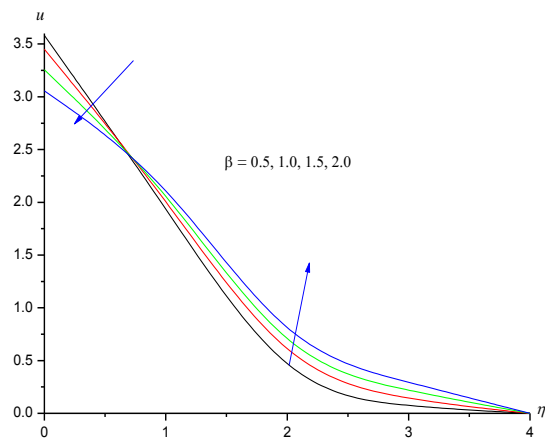


**Fig.6b** variation of temperature( $\theta$ )with  $Rd$   
 $Ra=2.0, Nr=0.5, M=0.5, \beta=0.5, \theta_r = -2,$

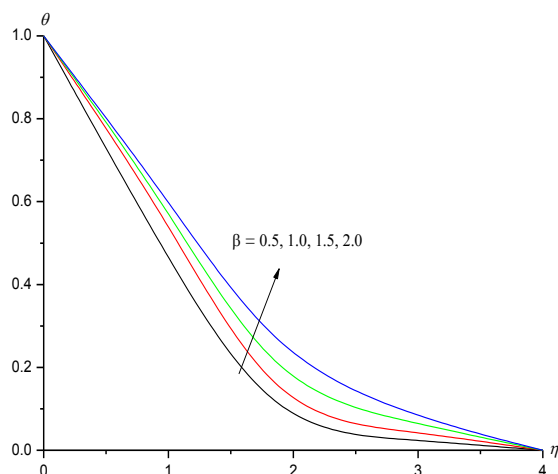




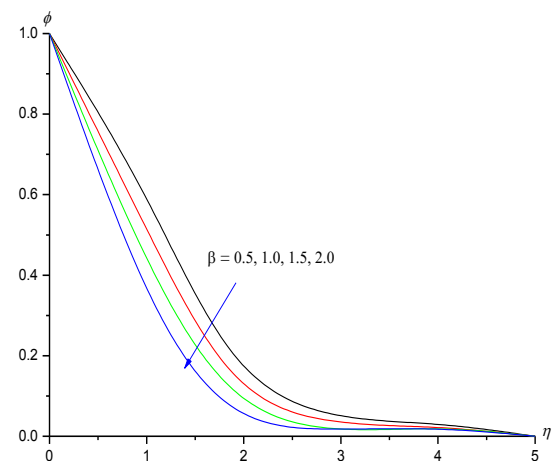
**Fig.7c** variation of Concentration( $\phi$ )with  $\theta r$   
 $M=0.5, Ra=2.0, Rd=0.5, \beta=0.5, Sc=0.24, Ra=2, a=0.2, \xi=\pi/4$



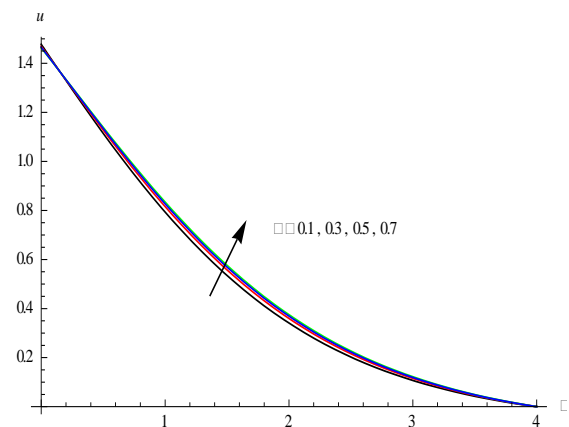
**Fig.8a** variation of axial velocity( $u$ )with  $\beta$   
 $M=0.5, Nr=0.5, Rd=0.5, \theta r=-2.0, Sc=0.24, Ra=2, a=0.2, \xi=\pi/4$



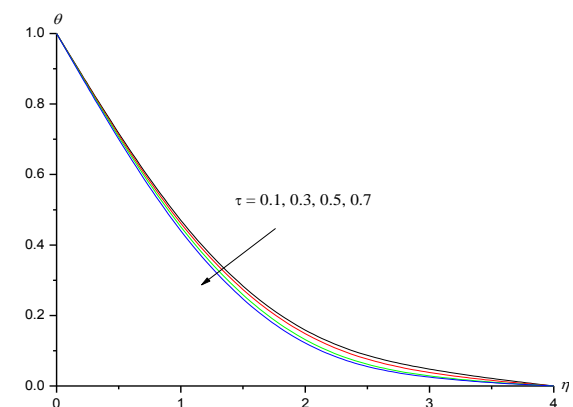
**Fig.8b** variation of temperature( $\theta$ )with  $\beta$   
 $M=0.5, Nr=0.5, Rd=0.5, \beta=0.5, \theta r=-2.0, Sc=0.24, Ra=2, a=0.2, \xi=\pi/4$



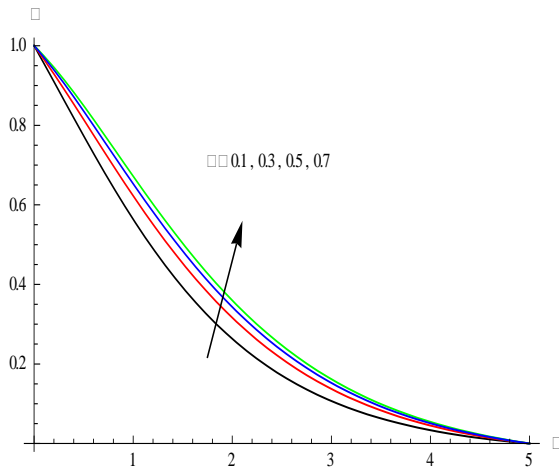
**Fig.8c** variation of Concentration( $\phi$ )with  $\beta$   
 $M=0.5, Nr=0.5, Rd=0.5, \beta=0.5, \theta r=-2.0, Sc=0.24, Ra=2, a=0.2, \xi=\pi/4$



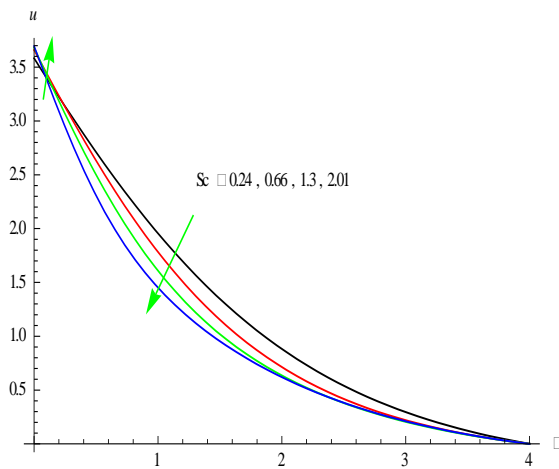
**Fig.9a** variation of axial velocity( $u$ )with  $\tau$   
 $M=0.5, Nr=0.5, Rd=0.5, \beta=0.5, \theta r=-2.0, Sc=0.24, a=0.2, \xi=\pi/4$



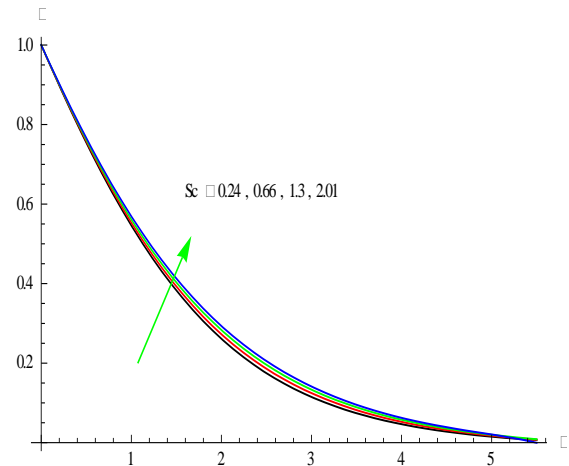
**Fig.9b** variation of temperature( $\theta$ )with  $\tau$   
 $Ra=2.0, Nr=0.5, Rd=0.5, \beta=0.5, \theta_r=-2.0,$   
 $Sc=0.24, a=0.2, \xi=\pi/4$



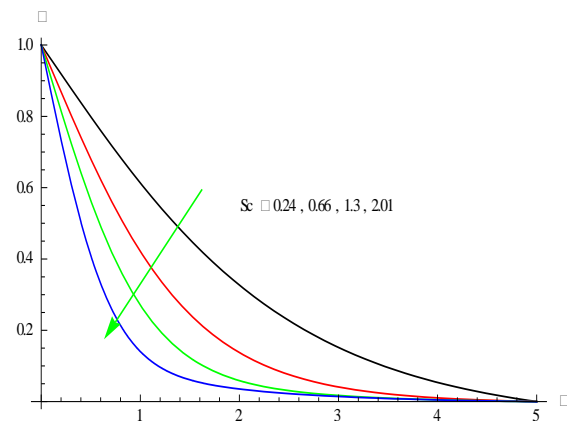
**Fig.9c** variation of Concentration( $\phi$ )with  $\tau$   
 $M=0.5, Ra=2.0, Rd=0.5, \beta=0.5, Sc=0.24,$   
 $Ra=2, a=0.2, \xi=\pi/4$



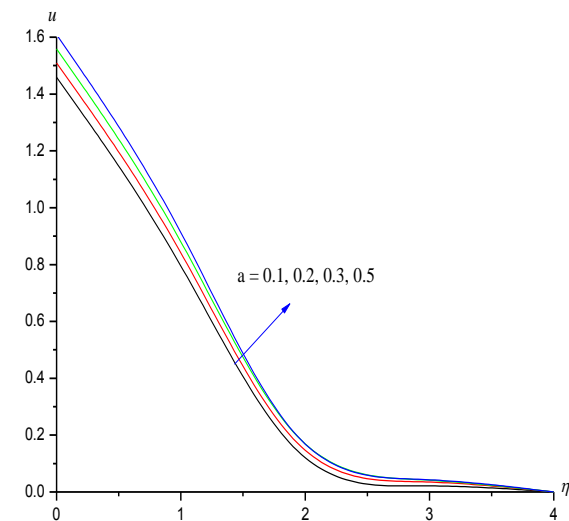
**Fig.10a** variation of axial velocity( $u$ )with  $Sc$   
 $M=0.5, Nr=0.5, Rd=0.5, \beta=0.5, \theta_r=-2,$   
 $Ra=2.0, a=0.2, \xi=\pi/4$



**Fig.10b** variation of temperature( $\theta$ )with  $Sc$   
 $Ra=2.0, Nr=0.5, Rd=0.5, \beta=0.5,$   
 $\theta_r=-2, M=0.5, a=0.2, \xi=\pi/4$

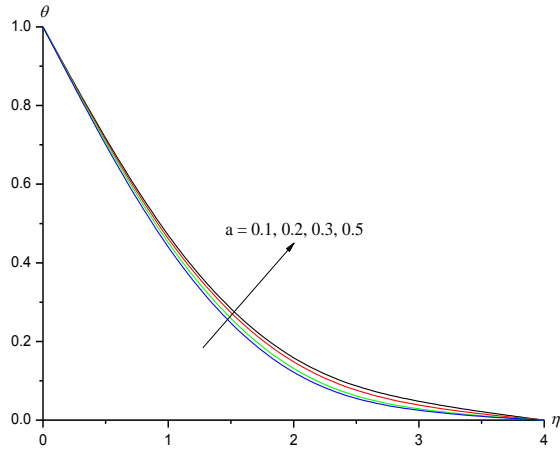


**Fig.10c** variation of Concentration( $\phi$ )with  $Sc$   
 $M=0.5, Ra=2.0, Rd=0.5, \beta=0.5,$   
 $Ra=2, a=0.2, \xi=\pi/4$



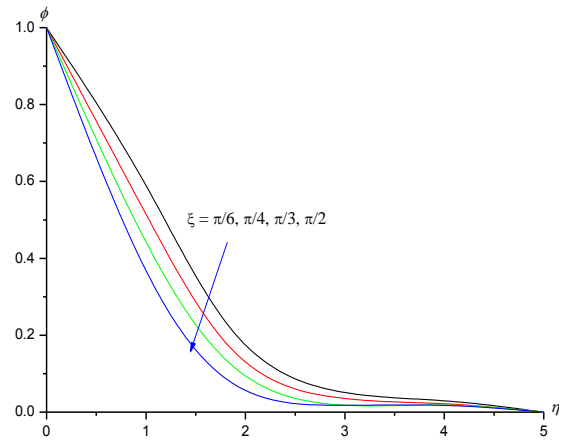
**Fig.11a** variation of axial velocity( $u$ )with  $a$

$M=0.5, Nr=0.5, Rd=0.5, \beta=0.5, Sc=0.24,$   
 $Ra=2.0, \theta_r=-2, Ra=2, \xi=\pi/4$

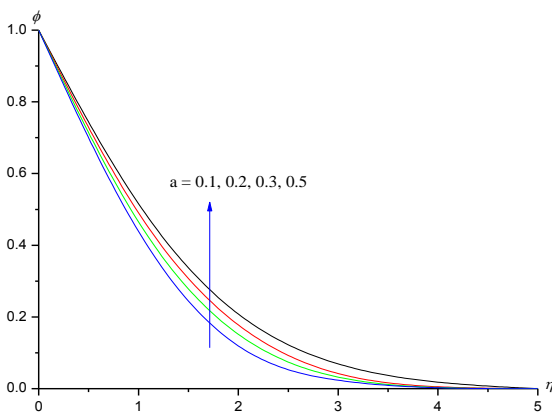


**Fig.11b** variation of temperature( $\theta$ )with a  
 $Ra=2.0, Nr=0.5, Rd=0.5, \beta=0.5, M=0.5,$   
 $Sc=0.24, \theta_r=-2, M=0.5, \xi=\pi/4$

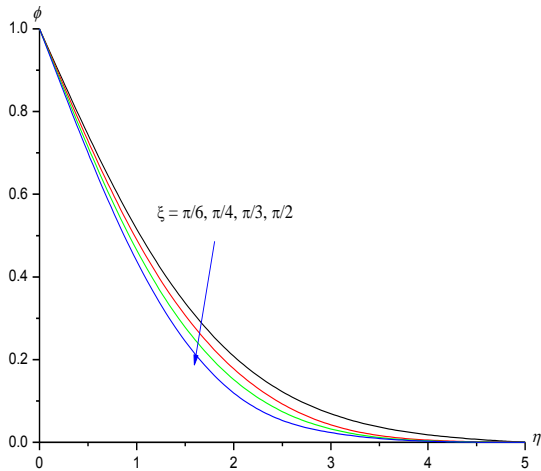
$M=0.5, Nr=0.5, Rd=0.5, \beta=0.5, \theta_r=-2,$   
 $Ra=2.0, Sc=0.24, a=0.2, Ra=2.0$



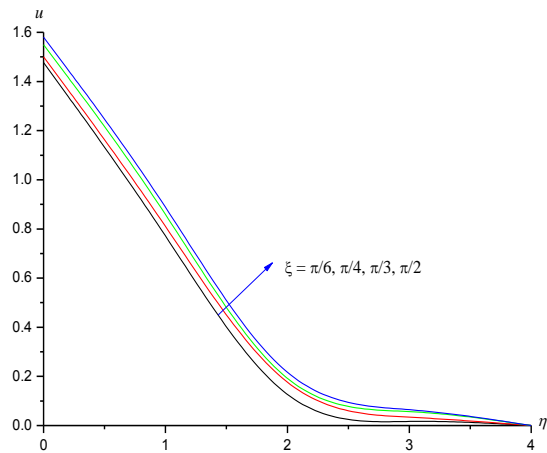
**Fig.12b** variation of temperature( $\theta$ )with  $\xi$   
 $Ra=2.0, Nr=0.5, Rd=0.5, \beta=0.5, \theta_r=-2,$   
 $M=0.5, Sc=0.24, a=0.2, M=0.5$



**Fig.11c** variation of Concentration( $\phi$ )with a  
 $M=0.5, Ra=2.0, Rd=0.5, \beta=0.5, Ra=2,$   
 $Sc=0.24, \theta_r=-2.0, \xi=\pi/4$



**Fig.12c** variation of Concentration( $\phi$ )with  $\xi$   
 $M=0.5, Ra=2.0, Rd=0.5, \beta=0.5, Ra=2,$   
 $M=0.5, Sc=0.24, a=0.2, \theta_r=-2.0$



**Fig.12a** variation of axial velocity( $u$ )with  $\xi$

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