

# Equilibrium, Kinetics and Thermodynamics of Hexavalent Chromium Adsorption onto Hen Eggshell from Aqueous Solution

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**ABSTRACT:** In this study, hen eggshell (HES) was employed as adsorbent for the removal of Hexavalent Chromium from aqueous solution. The study applied batch methods to investigate the equilibrium, kinetics and thermodynamics of the Hexavalent Chromium adsorption using HES. The equilibrium data was best fitted to the Freundlich adsorption isotherm model ( $R^2=0.998$ ) while the kinetic data was found to follow pseudo-second-order kinetic model ( $R^2 = 0.999$ ). The results of  $\Delta G^0$  and  $\Delta H^0$  showed that the adsorption process was feasible, non-spontaneous, and endothermic. The negative value of  $\Delta S^0$  describes decreasing degree of freedom and randomness during the adsorption process at the solid-liquid interface with some structural changes in the adsorbate and adsorbent.

**Key words:** Eggshell, Hexavalent Chromium, aqueous solution, equilibrium, kinetics, thermodynamics

## I. INTRODUCTION

The textile industry is well-known globally for huge water consumption and as one of the largest generators of industrial wastewater with high colour and dissolved organic compounds (Ahmad et al., 2011). Water pollution is a menace which major source is the indiscriminate discharge of untreated or poorly treated industrial effluents into the environment (Susu and Folami, 2014). In the textile industry, effluents from the dyeing and finishing processes are known to contain colour, a large amount of suspended organic solids and heavy metals such as Cr, Ni, and Cu (Ahmad et al., 2014).

Food wastes contain some valuable minerals which may be extracted so as to reduce the high cost of disposal of the environmental nuisance caused by such wastes (Ahmed et al., 2017).

Eggshell (ES) and eggshell membranes (ESM) are wastes produced in large quantities from sources such as poultries, homes, restaurants, bakeries and food manufacturing units. Each ES contains between 7000 and 17,000 pores (Zaman et al., 2018). Surface analysis of ES and ESM also revealed that they are porous materials and therefore can be employed as cost-effective adsorbents for the removal of hazardous chemicals thus, lessening the wastes going to landfill (Mopung and Jitchaijaronekul, 2017).

Eggshell has been used for purification of hydrogen generated for fuel cells (Mittal et al., 2016), adsorption of dye (Tsai et al., 2008) or heavy metals from wastewater (Guo et al., 2011) and CO<sub>2</sub> from combustion gases in a fluidized bed (Botome et al., 2017; Mohammadi et al., 2014). Other significant applications of eggshell include the production of thermoplastic materials such as high-density polyethylene to enhance rigidity, thermal stability and density of plastics. It is also being used to improve both physical and mechanical properties of soil, as well as renewable raw materials for catalyst synthesis in biodiesel production (Zaman et al., 2018; Tan et al., 2015).

Chromium and its compounds are toxic when introduced into natural water from a variety of industrial wastes. The major sources are from dyeing, electroplating, leather tanning, metal processing, paint and pigments, and the textile and steel fabrication industries (Al-Sou'od, 2013). These industries may release large quantities of toxic metal wastewater effluents above the permissible limit. The permissible limit for the discharge of Cr(VI) into inland surface water recommended by World Health Organization (WHO), Nigeria, India and US is 0.1mg/l and in potable water it is 0.05 mg/l (Mekonnen et al., 2015; [www.epa.gov/sdwa](http://www.epa.gov/sdwa); [www.nature.com](http://www.nature.com)). The

detrimental effects of Cr (VI) to biological systems and the environment had been well documented. Exposure to Hexavalent Chromium beyond the tolerance levels (0.05 mg/l) can have devastating effects on the human physiological, neurological and biological systems (Folami et al., 2019; Mishra and Gottipati, 2012).

In order to minimize this menace, a wide range of processes have been reported to remove heavy metals including Hexavalent Chromium from water and wastewater such as chemical precipitation (Kanagaraj et al., 2008), ion-exchange (Cavaco et al., 2007) and electrochemical methods (Liu et al., 2011). The application of such methods is costly and often lead to toxic sludge generation (Gholipour et al., 2011). However, adsorption had been reported as the most preferred due to its high efficacy, cost-effectiveness, versatility and easy handling (Mittal et al., 2016; Mishra and Gottipati, 2012).

In the present study, adsorption isotherms, kinetics and thermodynamics of Hexavalent Chromium removal from aqueous solution using hen eggshell as an adsorbent were evaluated.

## II. MATERIALS AND METHODS

**2.1 Materials:** The materials employed in this work include: Hen eggshell, de-ionized water, Chromium (VI) solution ( $K_2Cr_2O_7$ ), 0.1 M HCl, 0.1 M NaOH, digital weighing balance, isothermal water bath shaker, measuring cylinder, oven, screen, stop clock, 250 ml Erlenmeyer flasks, Atomic Adsorption Spectrophotometer (UNICAM 929, London).

**2.2. Preparation of Adsorbent (Hen Eggshell, HES):** The hen eggshell were collected from a local restaurant, washed thoroughly with de-ionized water to remove the dust and other stains and then dried in an oven at 85 °C for 30 minutes. The clean and dried HES were ground and screened to 120 – 150 µm particle sizes.

**2.3. Preparation of Stock and  $K_2Cr_2O_7(aq)$  Solutions:** A 5.0 g/l solution of chromium (VI) was prepared by dissolving 5.0 g of  $K_2Cr_2O_7$  in 1000 ml of de-ionized water. The solution was then converted to various  $K_2Cr_2O_7(aq)$  concentrations required for this work by diluting the initial stock solution (5.0 g/l  $K_2Cr_2O_7(aq)$ ) accordingly with de-ionized water.

**2.4. Batch Equilibrium Studies:** Different initial concentration (50, 100, 200, 300, 400 and 500 mg/l)  $K_2Cr_2O_7(aq)$  solution were investigated for the adsorption of  $Cr^{6+}$  ion onto HES in Batch equilibrium studies. In each case, 3.0 g of the HES

was added into 100 ml of the adsorbate ( $K_2Cr_2O_7(aq)$ ) in an Erlenmeyer flasks and pH adjusted to 2. Then, the flask was placed in an isothermal water bath shaker and subjected to the following process conditions: agitation speed 150 r.p.m., contact time 2 h and temperature 30 °C. After adsorption time was reached, the mixture was filtered to remove the adsorbent and the concentration of the  $Cr^{6+}$  ion in the filtrate in each case was determined using AA-Spectrophotometer.

The measure of the adsorption ( $Cr^{6+}$  removal) at equilibrium,  $q_e$  (mg/g), and  $Cr^{6+}$  percentage removal were evaluated using equation 2.1 and 2.2 respectively:

$$q_e = \frac{(C_o - C_e)V}{W} \quad 2.1$$

$$Cr(VI) \text{ ion } \% \text{ removal} = \frac{(C_o - C_e)}{C_o} \times 100 \quad 2.2$$

Where,  $C_o$  and  $C_e$  (mg/l) are the liquid-phase concentrations of  $Cr^{6+}$  at initial and at equilibrium respectively.  $V$  is the volume of the solution and  $W$  is the mass of HES used.

**2.5. Batch Kinetic Studies:** In the batch kinetic studies, 3 g of HES was added to 100 ml of 200 mg/l initial concentration with other process parameter kept constant. But, the measurement of the  $Cr^{6+}$  ion concentration was taken at preset time interval (30, 60, 90, 120, 150 and 180 mins). The quantity of  $Cr^{6+}$  ion uptake at any time,  $q_t$  (mg/g) was calculated using equation 2.3

$$q_t = \frac{(C_o - C_t)V}{W} \quad 2.3$$

Where,  $C_t$  (mg/l) is the liquid-phase concentration of  $Cr^{6+}$  at any arbitrary time,  $t$  (mins).

**2.6. Batch Thermodynamic Studies:** In order to obtain thermodynamic parameters, the adsorption process was studied at various temperature 25, 30, 45 and 55 °C through adjusting the temperature controller on the water bath shaker. Meanwhile, the concentration, adsorbent dose, contact time, solution pH and agitation speed used were 200 mg/l, 3 g, 2 h, 2 and 150 r.p.m. respectively in each case. The concentration of the  $Cr^{6+}$  ion left in the filtrate in each case was also determined using AA-Spectrophotometer.

## III. RESULTS AND DISCUSSION

### 3.1. Adsorption Isotherm

The adsorption isotherms are used to show how the adsorption molecules distribute between the solid phase and liquid phase at equilibrium

state. The Langmuir and Freundlich isotherms were considered in this work. The linear regression was used to determine the best-fitting isotherm and the significance of isotherm models compared by evaluating the correlation coefficients,  $R^2$ .

Langmuir's isotherm model is based on the theory that adsorption energy is constant and occurs on homogeneous surface by monolayer adsorption process. When the surface is covered by a monolayer of adsorbate, the adsorption goes on localized sites with no interaction between adsorbate molecules and that maximum adsorption

occurs (Ahmad, et al., 2014). The linear form of Langmuir isotherm equation is given as:

$$\frac{C_e}{q_e} = \frac{1}{Q_0 K_L} + \frac{1}{Q_0} C_e \quad 3.1$$

Where  $C_e$ (mg/l) is the  $Cr^{6+}$  ion equilibrium concentration and  $q_e$ (mg/g) is the amount of  $Cr^{6+}$  ion adsorbed per unit mass of HES.  $Q_0$ (mg/g) is the Langmuir constant related to adsorption capacity and  $K_L$ (l/mg) is rate of adsorption. The values of  $Q_0$ , and  $K_L$  were calculated from the intercept and slope of linear plot of  $C_e/q_e$  against  $C_e$  as depicted by Figure 3.1 and are presented in Table 3.1.

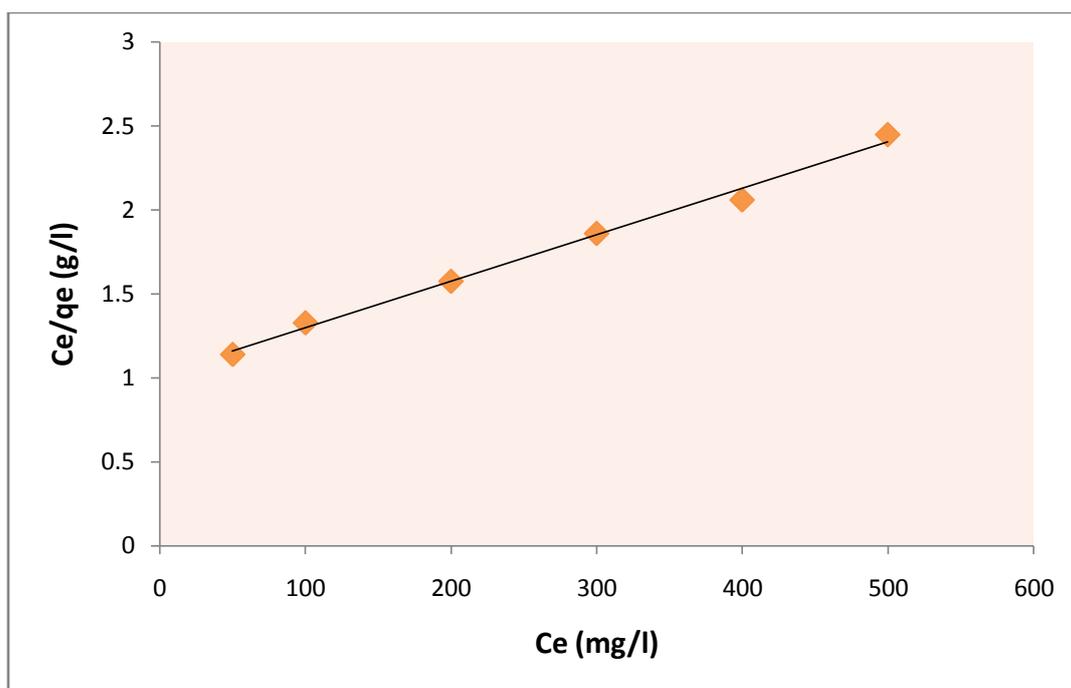


Figure 3.1: Plot of Langmuir Isotherm Model for  $Cr^{6+}$  ion Adsorption onto HES

Table 3.1: Langmuir and Freundlich Isotherm Parameters and Correlation Coefficient for the Adsorption of  $Cr^{6+}$  ion onto Hen Eggshell at 30 °C

Adsorbent	Langmuir Isotherm Parameters			Freundlich Isotherm Parameters		
	$Q_0$ (mg/g)	$K_L$ (l/mg)	$R^2$	$K_F$ (mg/g)	n	$R^2$
HES	228.53	0.322	0.931	3.96	2.619	0.998

Freundlich model is an empirical expression that is well-known relationship describing the sorption equation. It takes into account a heterogeneous surface and multilayer adsorption to the binding sites located on the surface of the sorbent (Mishra and Gottipati, 2012). The Freundlich model is expressed as:

$$\text{Log}q_e = \text{Log}K_f + \frac{1}{n} \text{Log}C_e \quad 3.2$$

Where  $K_f$  and  $n$  are indicative parameters of adsorption capacity and adsorption intensity respectively. As shown in Figure 3.2, the values of  $K_f$  and  $n$  were evaluated from the intercept and slope of the plot of  $\text{Log}q_e$  against  $\text{Log}C_e$  respectively. If  $n$  is greater than one, it implies that the adsorbate is favourably adsorbed on the adsorbent. The higher the value of  $n$ , the more favourable the adsorption and the stronger adsorption intensity (Ahmad and Alrozi, 2011).

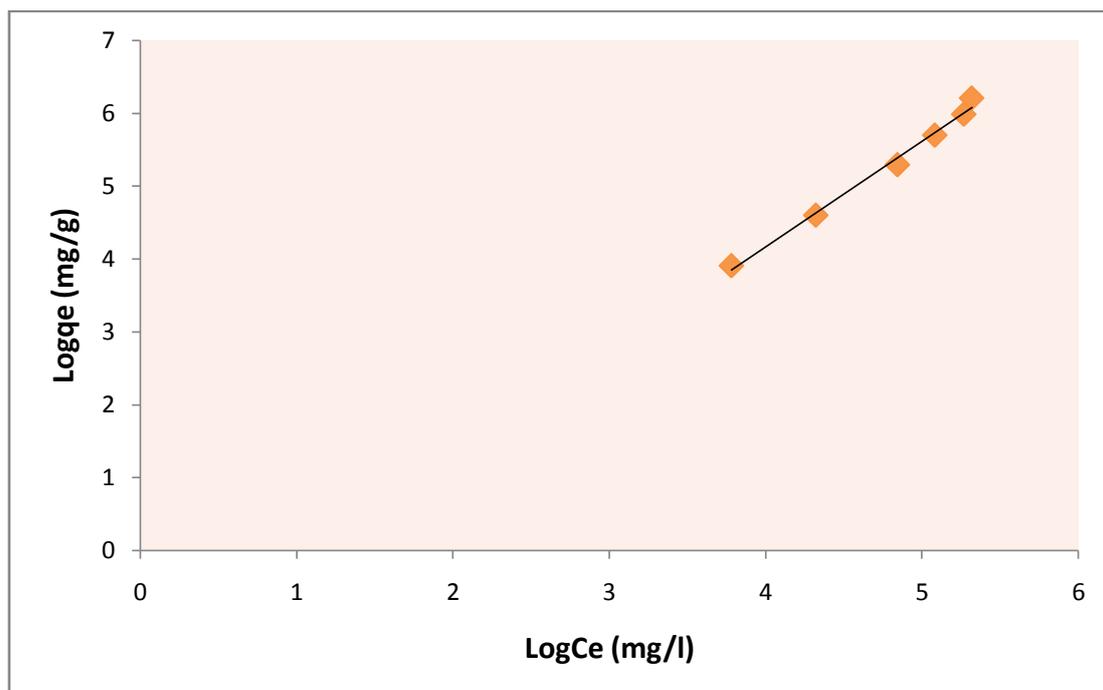


Figure 3.2: Plot of Freundlich Isotherm Model for Cr<sup>6+</sup> ion Adsorption onto HES

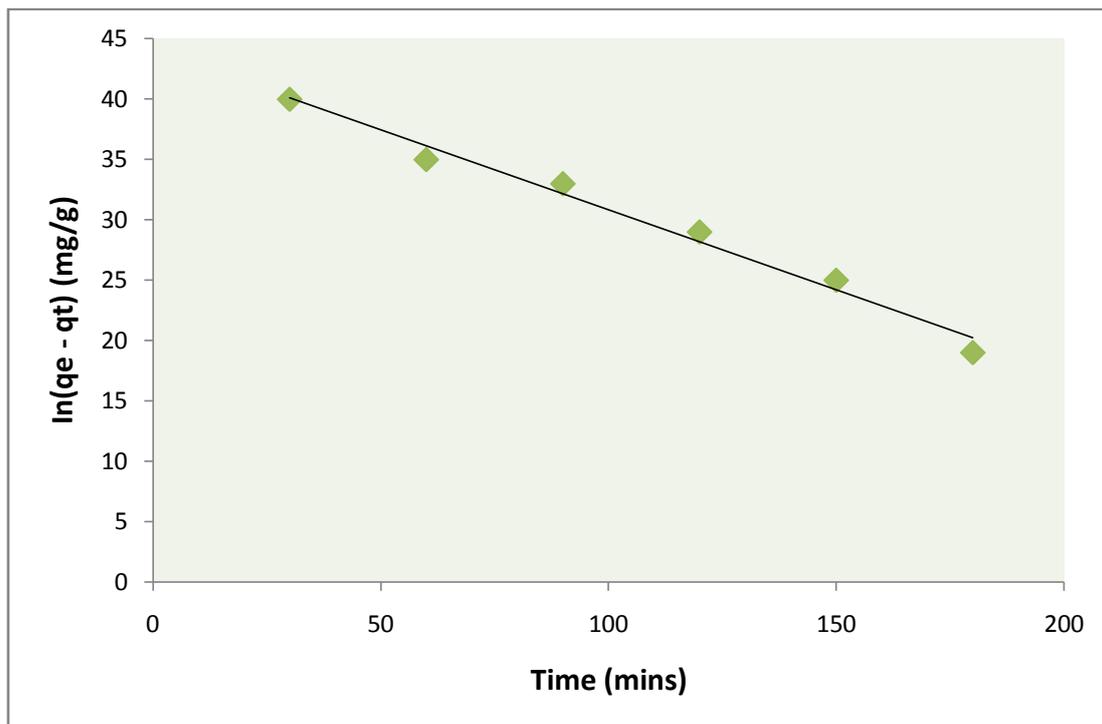
As provided in Table 3.1, Freundlich model gave higher R<sup>2</sup> value (0.998) than Langmuir model (0.931), which indicate that HES adsorption of Cr<sup>6+</sup> ion was made up of heterogeneous surface and multilayer adsorption (Gao et al., 2013). This outcome agreed with previous works on adsorption by activated carbon prepared from pinang frond (Ahmad et al., 2014), tea seed shells (Gao et al., 2013), mango nut (Kwaghger et al., 2012) and potato peel waste (Abdullah and Prasad, 2009).

### 3.2. Adsorption Kinetics

Kinetics adsorption data of Cr<sup>6+</sup> ion onto HES was analyzed using pseudo-first-order and pseudo-second-order. The pseudo first-order kinetic model is given by the equation 3.3 (Abdullah and Prasad, 2009):

$$\ln(q_e - q_t) = \ln q_e - k_1 t \quad 3.3$$

Where  $q_e$  and  $q_t$  (mg/g) are the amount of adsorbate adsorbed at equilibrium and at any time,  $t$  (min) respectively, and  $k_1$  (1/min) is the adsorption rate constant. Figure 3.3 shows that the linear plot of  $\ln(q_e - q_t)$  versus  $t$  gives a gradient of  $k_1$  and intercept at  $\ln q_e$ . Table 3.2 shows the values of  $k_1$  and  $R^2$  obtained from the plots at 30 °C, where the  $R^2$  value of pseudo-first-order model did not fit well with the range of contact time. In addition, the experimental  $q_e$  value did not match with the calculated value obtained from the linear plots. Thus, the adsorption of Cr<sup>6+</sup> ion onto HES was not following pseudo-first-order model and the kinetic data were further treated with the pseudo-second order kinetic model.



**Figure 3.3:** Plot of Pseudo-First Order Kinetic Model for Cr<sup>6+</sup> ion Adsorption onto HES

**Table 3.2:** Pseudo-First Order and Pseudo-Second Order Kinetic Parameters and Correlation Coefficients for the Adsorption of Cr<sup>6+</sup> ion onto Hen Eggshell at 30 °C

q <sub>e</sub> (mg/g) (exp.)	First Order Kinetic Parameters			Second Order Kinetic Parameters		
	q <sub>e</sub> (mg/g)	k <sub>1</sub> (l/min)	R <sup>2</sup>	q <sub>e</sub> (mg/g)	k <sub>2</sub> (g/mg.min)	R <sup>2</sup>
121.50	97.771	0.714	0.963	126.60	0.016	0.999

The pseudo-second-order model predicts the performance over the total range adsorption and is expressed as given by equation 3.4 (Mekonnen et al., 2015):

$$\frac{t}{q_t} = \frac{1}{k_2 q_e^2} + \frac{1}{q_e} t \quad 3.4$$

Where k<sub>2</sub>(g/mg.min) is the rate constant of second-order adsorption. Figure 3.4 showed that

the linear plot of t/q<sub>t</sub> versus t gave 1/k<sub>2</sub>q<sub>e</sub><sup>2</sup> as the intercept and 1/q<sub>e</sub> as the slope. In Table 3.2, the R<sup>2</sup> for the pseudo-second-order adsorption gave the higher value (0.999) which indicates that this kinetic model has a good relation and is consistent between the experimental and the calculated q<sub>e</sub> value. It also showed that the pseudo-second-order model adsorption is predominant.

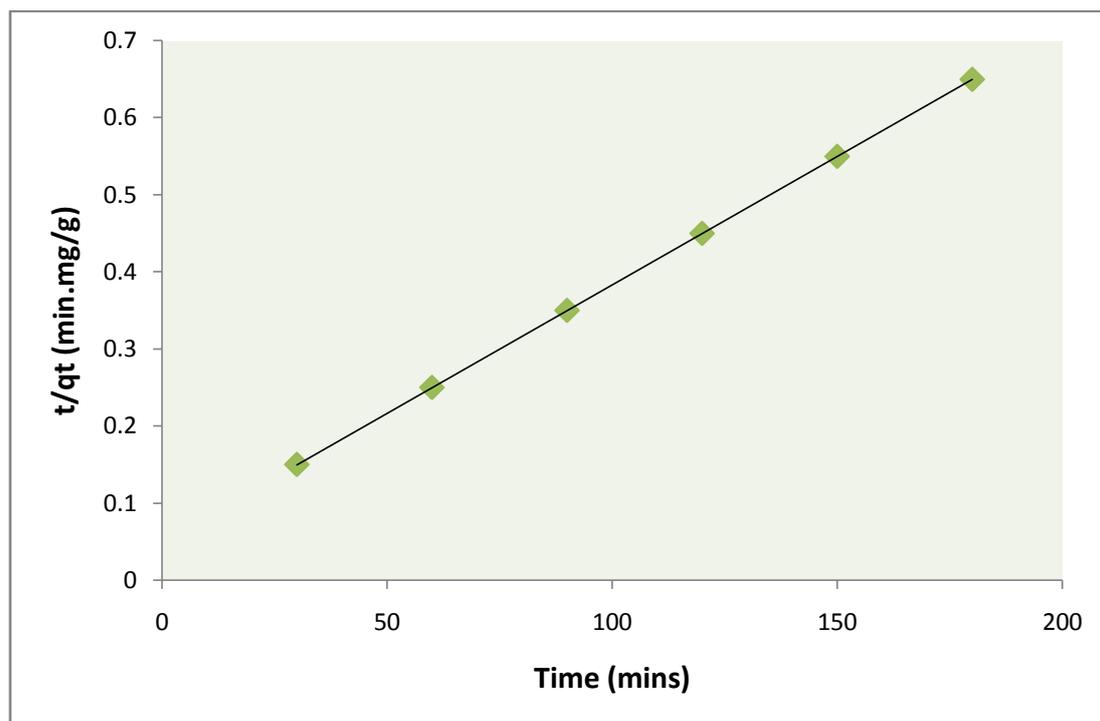


Figure 3.4: Plot of Pseudo-Second Order Kinetic Model for Cr<sup>6+</sup> ion Adsorption onto HES

### 3.3. Adsorption Thermodynamics

Thermodynamic parameters provide information of inherent energy changes associated with the adsorption process. The thermodynamic adsorption parameters determined were standard enthalpy change ( $\Delta H^0$ ), standard free energy change ( $\Delta G^0$ ), and standard entropy change ( $\Delta S^0$ ). The parameters are evaluated from the following equations (Mekonnen et al., 2015):

$$\ln K_L = \frac{\Delta S^0}{R} - \frac{\Delta H^0}{RT} \quad 3.5$$

$$\Delta G^0 = -RT \ln K_L \quad 3.6$$

Where R(8.314 J/mol.K) is the universal gas constant, T (K) is the absolute solution temperature, and  $K_L$ (l/mg) is the Langmuir isotherm constant.  $\Delta H^0$  and  $\Delta S^0$  were evaluated from the slope and intercept of the linear plot of  $\ln K_L$  versus  $1/T$  respectively. To obtain the activation energy of adsorption, Arrhenius equation was employed:

$$\ln k_2 = \ln A - \frac{E_a}{RT} \quad 3.7$$

Where  $k_2$ (g/mg h) is the rate constant obtained from the pseudo-second-order kinetic model,  $E_a$ (kJ/mol) is the Arrhenius activation energy of adsorption and A is the Arrhenius factor. When  $\ln k_2$  was plotted against  $1/T$ , a straight line with gradient of  $-E_a/R$  was obtained.

Table 3.4: Thermodynamic Parameters for the Adsorption of Cr<sup>6+</sup> ion onto HES

$\Delta H^0$ (kJ/mol)	$\Delta S^0$ (J/mol.K)	$E_a$ (kJ/mol)	$\Delta G^0$ (kJ/mol)			
			298 K	303 K	318 K	328 K
7.85	-10.92	8.98	8.75	9.90	10.85	11.50

$\Delta H^0$ ,  $\Delta S^0$ ,  $\Delta G^0$  and  $E_a$  for the adsorption of Cr<sup>6+</sup> ion onto HES are reported in Table 3.4. The positive value of  $\Delta H^0$  showed that the adsorption of Cr<sup>6+</sup> ion onto HES was endothermic in nature, which supported the observation made during batch thermodynamic studies where the Cr<sup>6+</sup> ion removal increase with increase in solution temperature. The negative value of  $\Delta S^0$  describes decreasing degree

of freedom and randomness during the adsorption process at the solid-liquid interface with some structural changes in the adsorbate and adsorbent. Similar trends had also been reported in the adsorption of Zinc by walnut shell (Oladadehan et al., 2018), Hexavalent Chromium by potato peel waste (Abdullah and Prasad, 2009) and direct dyes by carbon nanotubes (Kuo et al., 2008).

$\Delta G^0$  value was positive which depicted the condition of non-spontaneous nature of the process at the range of temperature studied. The  $E_a$  value was positive and lower than 40 kJ/mol indicating the feasibility of the adsorption process and that the adsorption was physically controlled respectively (Ahmad et al., 2014).

#### IV. CONCLUSION

In the textile industry, effluents from the dyeing and finishing processes are known to contain colour, a large amount of suspended organic solids and heavy metals such as Cr, Ni, and Cu. It has been widely reported that the exposure to Hexavalent Chromium beyond the tolerance levels (0.05 mg/l) can have damaging effects on the human physiological, neurological and biological systems. In this study, batch methods were used to investigate the equilibrium, kinetics and thermodynamics of the Hexavalent Chromium adsorption using hen eggshell. The equilibrium data was best fitted to the Freundlich adsorption isotherm model. The results of kinetic models showed that the pseudo-second-order kinetic model correlate well to the experimental data. The results of the thermodynamic parameters showed that the adsorption process was feasible, non-spontaneous, and endothermic. The negative value of entropy describes decreasing degree of freedom and randomness during the adsorption process at the solid-liquid interface with some structural changes in the adsorbate and adsorbent.

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