

# Development of a Model to Alleviate Flooding in oko-Erin area, Kwarastate

Adeyokunnu, A.T.<sup>1\*</sup> Oyelami, A.K.<sup>2</sup>

<sup>1</sup>Department of Civil Engineering, Ajayi Crowther University, Oyo, Oyo-State, Nigeria.

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## ABSTRACT:

Floods and its impact on both individuals and communities have social, economic and environmental consequences. The aim of this study is development of intensity duration frequency in Oko-Erin, to mitigate frequent events of flooding in the area. Thirty (30) years rainfall data of Ilorin metropolis, obtained from Nigeria Meteorological Station Kwara State for runoff computation of the catchment

area. The annual monthly average rainfall moving averages were computed and thereafter graphs drawn to show the overall trend over the 30-year period. Furthermore, the Log-Pearson Type III distribution was used to fit the frequency distribution data to predict the design flood for a river at some site by estimating mean ( $\mu$ ) and Standard deviation ( $\sigma$ ) from 10 to 120 minutes. Flood routing model of the area was developed and calibrated. The maximum rainfall data for Ilorin has a  $R^2$  value of 0.9125. The mean and standard ranged 64.61-320.21 and 20.84 - 103.59, respectively and computed Runoff varied from (281.61-1444.61)  $\text{mm}^3$ . Also, 10 minutes' duration is notably of higher intensity than the longer duration rainfall. The calibrated flood routing model on the study area was  $xT = 122.47 \ln(\text{Tr}) + 205.17$ . The developed curve can be useful for flood forecasting in Ilorin metropolis

**KEYWORDS:** Development, Model, Alleviate, Flood Routine, Rainfall Intensity and Log Pearson Type III.

## I. INTRODUCTION

Flood is a major natural hazard with often immeasurable impact, affecting annually 170 million people therefore, flood risk management needs to overcome national borders, geographic location and socio-economic limitations. Flooding is one of the main natural hazards jeopardizing lives and properties of the people, and causing relevant economic losses (Ciampa et al., 2021). Flood risk management

is usually divided into flood risk assessment and flood risk mitigation. This distinction takes into account apart from the hazard also its impact, since the total elimination of risk is neither possible nor efficient (Kazakis et al., 2015). Indisputably, strategies against floods' impact at a regional scale require the identification of prone areas to provide early warning, facilitate quick response and decrease the impact of possible flood events (Biswas, 2018).

It is noted that in spite of extensive research on river flooding, urban flooding has not been considered extensively important and is yet to be studied. In particular, among developing countries, urban flood planning and management is often carried out by using traditional approaches, such as channelization (discharging the rainwater into the channel network), without consideration of novel techniques (source control approaches) such as Low-Impact Development (LID) and best management practices (BMPs).

It is, therefore, necessary to study the capabilities of novel storm water measures such as detention basins for urban flood control in developing countries (Gesare et al., 2016).

Removal of excess storm water is of utmost importance and concern for every community. Flood control measures sometimes concentrate on retention or detention of the same extreme storm event. This requirement is usually specific to a single basin with the goal of containing a certain storm event flow volume retention or obtaining a specific peak flow reduction detention (Travis & Mays, 2008). Therefore redesigning flood control structures in isolation will worsen the situation rather than providing solution to the problem (Ahmadisharaf et al., 2016). For instance, Ravazzani et al., (2014) noted that a single detention pond will tend to offset the time of concentration and reduce the peak flow of its contributing watershed. However, the resulting outlet hydrograph can combine with the other watershed flows in the region to produce flows that are more damaging than the pre-developed condition.

Frequencies of extreme flood events were increased in line with the global climate change (Sari et al., 2018). An alternative to detention is to require every site to retain its own storm-water runoff. Various studies have shown that retention basins are successful flood control measures, particularly for pervious soils and frequent storm. Unlike detention basins, retention basins typically use infiltration as their primary means of storm-water disposal and thus are referred to as infiltration basins. Retention basins are defined as flood control ponds wet or dry designed to store water to mitigate flooding, and infiltration

is assumed the only means of outlet flow of the stored water. The presented model in this study is flexible and can incorporate evaporation or bleed off structures if needed without undue difficulty.

At present, no attention is paid on model for flood routing of Oko-Erin, this call for concept development of Intensity Duration Frequency Curve.

## II. MATERIALS AND METHODS

### 2.0 Description of Study Area

Oko-

Erin Community is located in the Ilorin West Local Government Area of Kwara State, Nigeria about 327 km West of Abuja, the country's capital town. The Community is bordered by Taiwo and Saw-Mail/Osere Communities. It is one of the densely populated and well-known community in the Ilorin Metropolis as it houses notable institutions such as Government Girls Day Secondary School, Oko-Erin, Atoto Press Plc to mention but a few and it is closer to the Ilorin International Airport. Map of Oko-Erin and its environs is presented in Figure 2.1. Over the years, the area is known with cases of flooding due to other factors, which often not had led to flooding, which leads to loss of lives and properties in the community. One major factor that is likely responsible for the incessant flooding in the area is the dumping of refuse in drainages system or buildings on waterways, which lead to erosion of bridges in the area.



Figure 2.1: Map showing Oko-Erin and its environs.

### 2.1 Temporal Variation of Rainfall Intensity in Oko-Erin

In this study, Annual Maxima Series was used for plotting of the IDF curves. The values of the annual maxima precipitation from a given area for a number of years constitute a hydrologic data series called the annual maxima series. The data are arranged in decreasing order of magnitude and the probability of each event being equaled to or exceeded (plotting position) was calculated by plotting-position formula. Weibull's plotting-position

formula was used for frequency studies involving hydrologic parameters.

The magnitudes of yearly maximum rainfall depths corresponding to storm durations 24hrs, 48hrs, etc. for all past years for which data is available. Various hourly magnitudes of rainfall for each year were considered to identify the maximum rainfall in continuous time duration and rainfall depths were arranged in decreasing order of magnitudes. These were repeated for other continuous durations of 48, 72, 96

and 120hrs. The formula for Frequency Distribution Function is expressed in Equation 2.1:

$$x_t = \bar{x} + k\sigma \quad 2.1$$

Where,

$x_t$  = value of the variate of a random hydrologic series with a return period  $T$ ,  
 $\bar{x}$  = mean of the variate,  
 $\sigma$  = standard deviation of the variate,

The collected rainfall data for Ilorin were fitted with a probability density function and Extreme Value Gumbel Type I distribution which is commonly used for rainfall analysis for a given rainfall duration 't'. The Extreme Value Type I distribution frequency factor for annual maximum rainfall depth is expressed in Equation 2.2:

$$k = \left( \frac{\sqrt{6}}{3t^{1/4}} \right) \left( 0.2 + \log_e \log_e \frac{T}{T_h} \right)$$

Rainfall depths were calculated using K value for various frequencies of occurrence for various durations. The depths were converted to rainfall intensities by dividing the rainfall depths (mm)

with durations (hr). Thus, set of values of rainfall intensities were generated for corresponding set of durations and drawn using spreadsheet software. The equations of these curves were determined. The trend line function found in any spreadsheet equation of the curve, with the  $R^2$  value were determined. The obtained equations were obtained in the form shown in equation 2.3

$$i = at^{*b} \quad 2.3$$

From this the parameters, (a,b) were determined. With the parameters determined, the intensity of rainfall for any duration for a given return period were determined.

### 2.3.1 Rainfall-Runoff Computation

The monthly and the annual average rainfall were computed for the years. The graph showing trends of rainfall intensities were drawn. According to the World Meteorological Organization, in the absence of a climatological standard, provisional for normal can be computed from at least 10-12 years of the prior observation taken before the period under review.

In this case, average rainfall records used were

from Nigerian meteorological station for Ilorin which had observations from 1989-2019, therefore the normal was computed for a 30-year period and was used as the baseline. The average rainfall were computed for each month within the period to obtain the annual and monthly anomalies. Rainfall runoff was computed by multiplying the rainfall intensity, runoff coefficient and Catchment Area.

### 2.4 Rainfall Distribution using Log-Pearson Type III

The Log-Pearson Type III distribution is a statistical technique for fitting frequency distribution data to predict the design flood for a river at gauged site. Once the statistical information is calculated for the river site, a frequency distribution were constructed. The probabilities of floods of various sizes were extracted from the curve. The extrapolation of the values for events with return periods were beyond the observed flood events (Satheet al., 2012). The Log-Pearson Type III distribution is calculated using the general Equation 2.1.

Where  $k$  = frequency factor determined from Gamma and Log-Pearson Type III Distributions table. However, the Log Pearson Type III distribution of  $X$ , which has been widely adopted to reduce skewness, is equivalent to applying Log Pearson Type III to the transformed variable  $\log X$  as shown in Equation 2.4

$$\log X = \bar{\log X} + K\sigma_{\log X} \quad 2.4$$

Where  $X$  is the flood discharge value of some specified probability,  $\bar{\log X}$  is the average of the  $\log X$  discharge values,  $K$

is frequency factor.  $\sigma_{\log X}$  is the standard deviation of  $\log x$  values.

The frequency factor  $K$  is a function of skewness coefficient and return period and can be read from published tables developed by integrating the appropriate probability density function. The flood magnitude for various return periods is found by solving the general equation. The mean, standard deviation and skewness coefficient are presented in Equations 2.5– 2.7.

$$\bar{\log X} = \frac{\sum \log X}{n} \quad 2.5$$

$$\sigma_{\log X} = \left[ \frac{\sum (\log X - \bar{\log X})^2}{(n-1)} \right]^{1/2} \quad 2.6$$

$$g = \frac{\sum (\log D - \bar{\log D})^2}{(n-1) s^2} \quad 2.7$$

Where  $n$  is the number of entries of  $X$ ,  $\log \bar{D}$  is the average of the  $\log x$  discharge value. The Log Pearson Type III distribution is given in Equation 2.8

$$T = \frac{n+0.2}{m+0.4}$$

where  $n$  is the number of years of record,  $m$  is the rank obtained by arranging the annual flood series in descending order of magnitude with the maximum being assigned the rank of 1.

### III. RESULTS AND DISCUSSION

#### 3.0 Rainfall Variation in Eko-Erin

The rainfall trend in Ilorin between the year 1989–2019 is presented in Figure 3.1. The average rainfall intensity from January to December as shown in Figure 3.2. The month of September has the maximum rainfall.

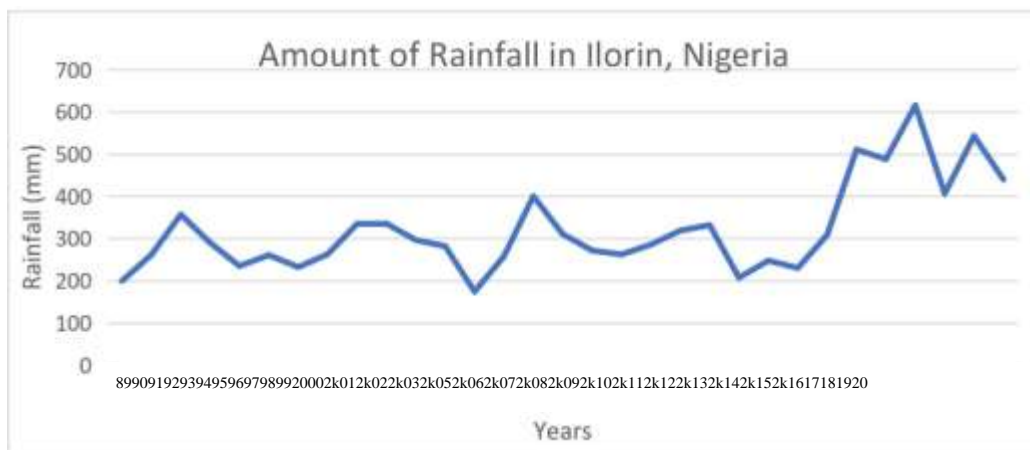


Figure 3.1: Distribution of the Amount of Rainfall from 1989–2019

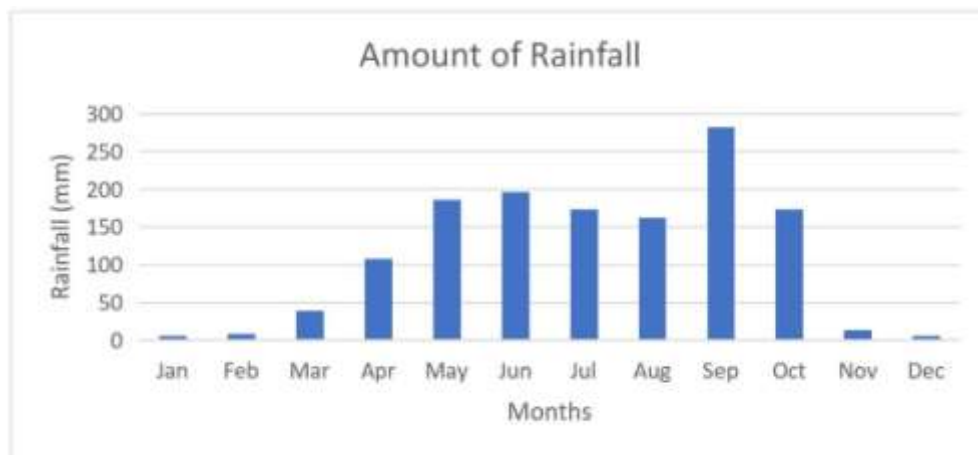


Figure 3.2: Distribution of the Amount of Rainfall from January–December

#### 3.1 Distribution of Rainfall Data using Log-Pearson Type III

The maximum rainfall data in Ilorin showed a high correlation on the Log-Pearson Type III distribution. It was observed that maximum rainfall data for Ilorin has a  $R^2$  value of 0.9125 when fitted to the model. The probability plot for Log-

Pearson Type III is shown in Figure 3.3.

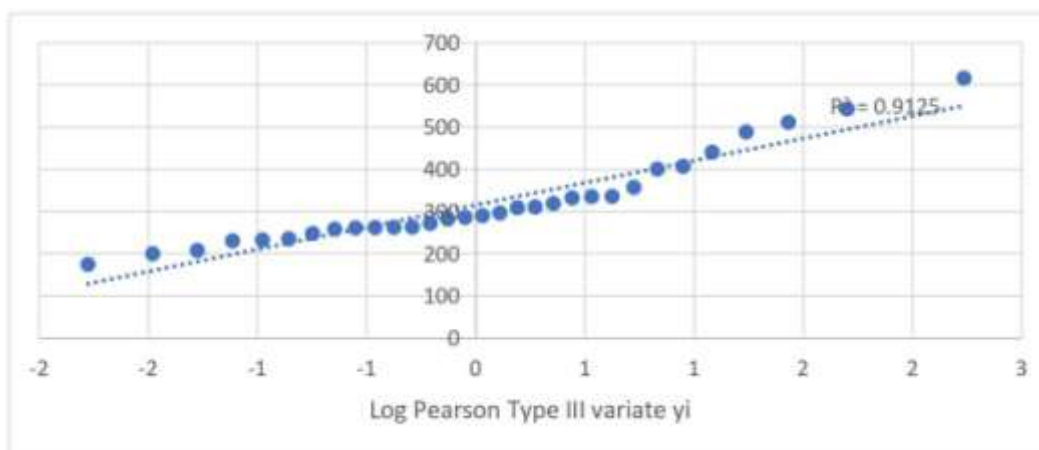


Figure 3.3: Probability Plot for Ilorin Metropolis

After the result of the analysis of best fit were completed, Log-Pearson Type III distribution model with highest  $R^2$  value was used to estimate the expected rainfall amount by first estimating frequency parameters  $\sigma$  and  $\mu$  for each of the durations. The resulting parameters are shown in

Table 3.1. Subsequently, the expected maximum rainfall intensity for Ilorin in mm/hr was calculated using return periods of 2, 5, 10, 25, 50 and 100 years. The results are represented in Tables 3.2-3.4 for durations 10, 20, 30, 60, 90 and 120 minutes.

Table 3.1: Computed Log Pearson III Statistical Parameters for Ilorin

Parameters	Duration	10min	20min	30min	60min	90min	120 min
Total Data	n	31	31	31	31	31	31
Mean Value	$\mu$	64.61	98.50	126.05	192.15	245.85	321.10
Standard Deviation	$\sigma$	20.84	31.78	40.66	61.99	79.31	103.59

Table 3.2: Rainfall Depth Computed from Log-Pearson III Model for Ilorin

Ilorin Rainfall Amount (mm)						
Duration	Return Periods					
	2 Years	5 Years	10 Years	25 Years	50 Years	100 Years
10min	61	80	92	107	119	130
20min	93	121	140	163	181	198
30min	119	155	179	209	231	254
60min	182	237	273	319	353	387
90min	233	303	349	408	451	495
120min	304	396	456	533	590	646

### 3.4 Flood Routine Model

The result in Table 3.1 and 3.2 implies that mean value and standard deviation values is increasing as the duration at different return period increased. This is similar to previous work of (Ciampa et al.,2021).

Figure 3.4 shows the computed rainfall intensity-frequency for Ilorin in the linear logarithm form. This was obtained by plotting rainfall intensity values from the Log-Pearson Type III Distribution against the return periods. Equations derived from the plot are shown in Table 3.5. The

equations were used to estimate rainfall intensity for the durations at different return periods that could accurately read off the IDF curve. Ten (10) minutes' duration is notably of higher intensity than the longer duration rainfall. This suggests that early stage of rainfall is of higher intensity and the rainfall decreases in intensity as its duration progresses. Figure 3.5 and Figure 3.6 shows graphical representation frequency of occurrence and intensity rainfall curve plotted respectively.

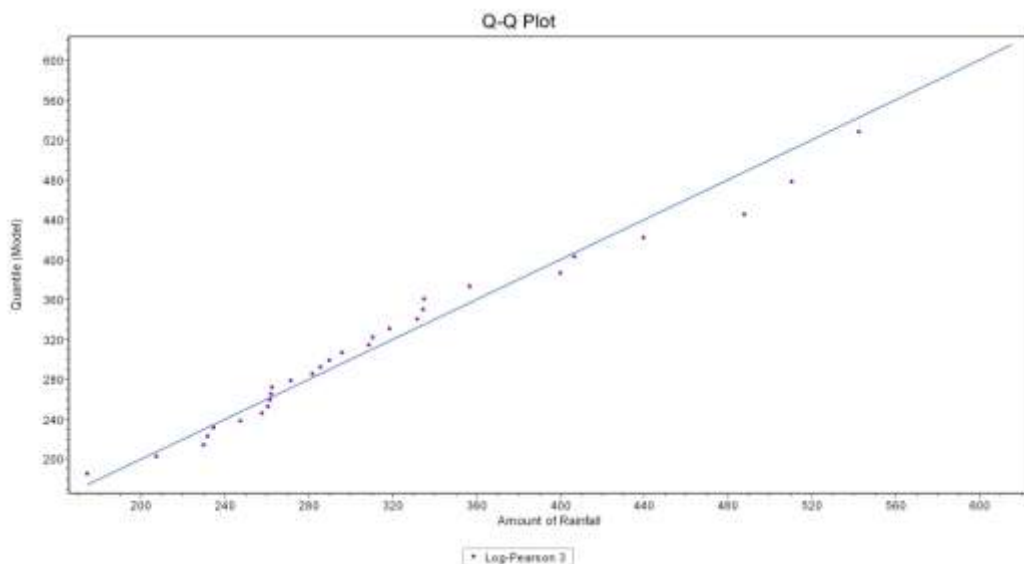


Figure 3.4: Q-Q Plot Displaying the Fitted Log-Pearson Type III of the Amount of Rainfall

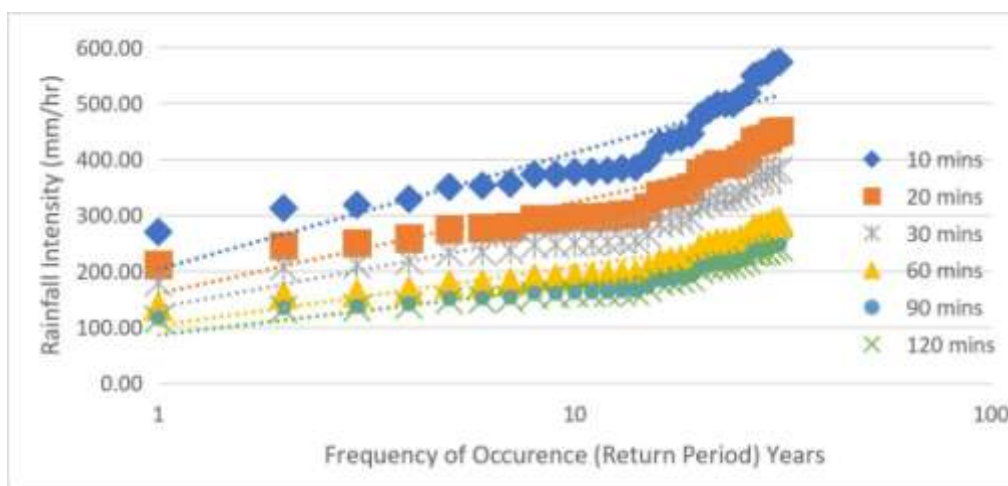


Figure 3.5: Rainfall Intensity Frequency Curve for Ilorin

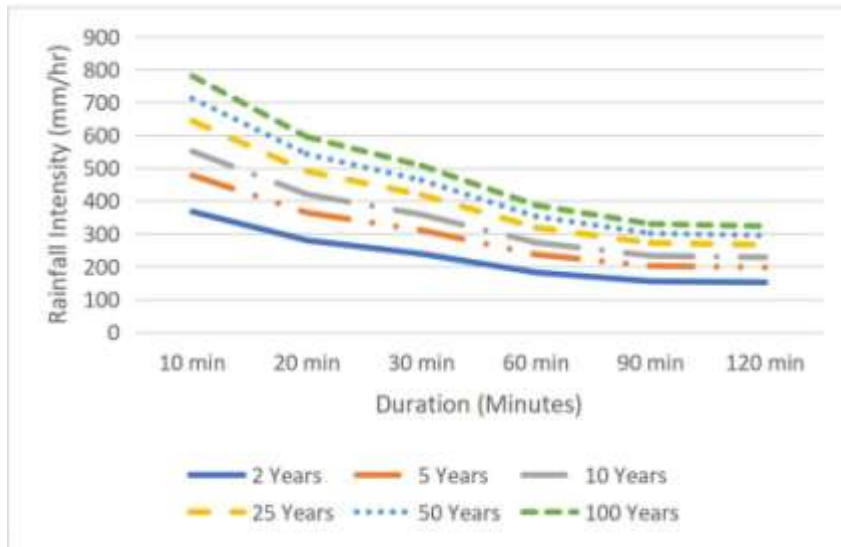


Figure 3.6: IDF Curve for Ilorin

Table 3.3: Model Flood Routing within the Catchment using Log-Pearson Type III Model

Duration (Minutes)	Log-Pearson III Model
10	$x_T = 24.642 \ln(T_R) + 41.283$
20	$x_T = 37.568 \ln(T_R) + 62.938$
30	$x_T = 48.075 \ln(T_R) + 80.539$
60	$x_T = 73.288 \ln(T_R) + 122.78$
90	$x_T = 93.766 \ln(T_R) + 157.08$
120	$x_T = 122.47 \ln(T_R) + 205.17$

Table 3.4: Rainfall Intensity Computed from Log-Pearson III Model for Ilorin

Ilorin Rainfall Amount (mm/hr)						
Duration	Return Periods					
	2 Years	5 Years	10 Years	25 Years	50 Years	100 Years
10 min	367	478	551	643	712	780
20 min	280	364	420	490	543	595
30 min	239	311	358	418	463	507
60 min	182	237	273	319	353	387
90 min	155	202	233	272	301	330
120 min	152	198	228	266	295	323

Table 3.5: Peak Runoff within the Catchment using 30 Years Rainfall Intensity Data

Ilorin Rainfall Runoff (Qp)						
Duration	Return Periods					
	2 Years	5 Years	10 Years	25 Years	50 Years	100 Years
10 min	679.975	884.6832	1020.218	1191.466	1318.508	1444.612
20 min	518.326	674.3693	777.6836	908.2215	1005.062	1101.187

<b>30min</b>	442.1904	575.3129	663.4517	774.8152	857.431	939.4367
<b>60min</b>	337.047	438.5158	505.6971	590.5807	653.5522	716.0588
<b>90min</b>	287.482	374.0292	431.331	503.732	557.4431	610.7577
<b>120min</b>	281.6142	366.3949	422.5271	493.4503	546.0652	598.2915

#### IV. CONCLUSION

The following conclusions were drawn from the study:

- (i) The intensity-duration-frequency curves was plotted and generated equations were used to estimate rainfall intensity for the durations at different return periods.
- (ii) The 10 minutes' duration is notably of higher intensity than the longer duration rainfall. This suggests that early stage of rainfall is of higher intensity and the rainfall decreases in intensity as its duration progresses.
- (iii) The maximum rainfall data in Ilorin showed a high correlation on the Log-Pearson Type III distribution.

Recommendation from the Study

The following recommendation were made from obtained result in this study

- (i) The developed IDF Curve can be used as a baseline report for flood studies in Ilorin metropolis.
- (ii) The estimated discharge can be used for redesigning of failed hydraulic structures in Oko Erin catchment.

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